

# **Storm Water Flow Study Report**

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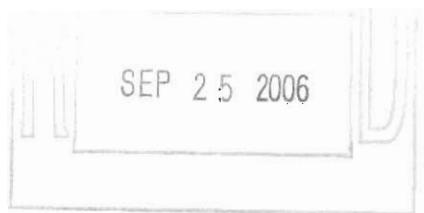
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## 1.0 Introduction

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The following sections provide a description of the methodology to be used to characterize and document the storm water runoff generated by the drainage basins for unnamed tributaries to Flat Creek upstream of the El Dorado Chemical Company facility (EDCC). A vicinity map outlining the upstream drainage basins and showing the location of the National Pollutant Discharge Elimination System (NPDES) permitted outfalls on the EDCC property is included as Figure 1.

Water level and flow data will be collected during storm events to develop a rating curve to represent the background stream flow. GBM<sup>c</sup> & Associates, Bryant, Arkansas (GBM<sup>c</sup>) will provide the functional team that will conduct the fieldwork, sampling, and data analysis for the Flat Creek tributary drainage basin characterization.

The final project report, including all calculations, data evaluation and discussion of findings will be delivered to EDCC for review, then will be submitted to the Arkansas Department of Environmental Quality (ADEQ) Water Division.

The proposed study is scheduled to occur over a twelve-month period during 2004-2005. The minimum number of runoff events necessary to provide an adequate data set is twelve. If twelve runoff events do not occur during the twelve-month duration of the proposed study, then the study may be extended to capture the necessary events. However, if more than twelve events occur over the duration of the proposed study, flow measurements will be collected from as many runoff events as practicable.

## **1.0 Introduction**

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The following sections provide a description of the methodology used to characterize and document the storm water runoff generated by the drainage basin for the unnamed tributaries to Flat Creek upstream of El Dorado Chemical Company (EDCC) and the results of the characterization. A vicinity map outlining the upstream drainage basins and showing the location of the National Pollutant Discharge Elimination System (NPDES) permitted outfalls on the EDCC property is included as Figure 1.

The July 15, 2004 Storm Water Flow Study Plan (the Plan) identified the characterization objectives and tasks to complete the study. This characterization report deviates from the Plan, due to the permanent abandonment of EDCC Outfalls 004 and 005 which discharged to the south unnamed tributary. Because there will be no future discharges from these two locations, the data collected for the south tributary and associated outfalls was not analyzed and the findings presented in this report are only for the north unnamed tributary and Outfalls 006 and 007.

Water level and flow data were collected during storm events to develop a rating curve to represent the north tributary background stream flow. Recorded water levels used in this study are included as Appendix A.

## **2.0 Project Organization**

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GBM<sup>c</sup> & Associates, Bryant, Arkansas (GBM<sup>c</sup>) provided the functional team that conducted the fieldwork and data analysis for the north tributary drainage basin characterization and the EDCC outfalls.

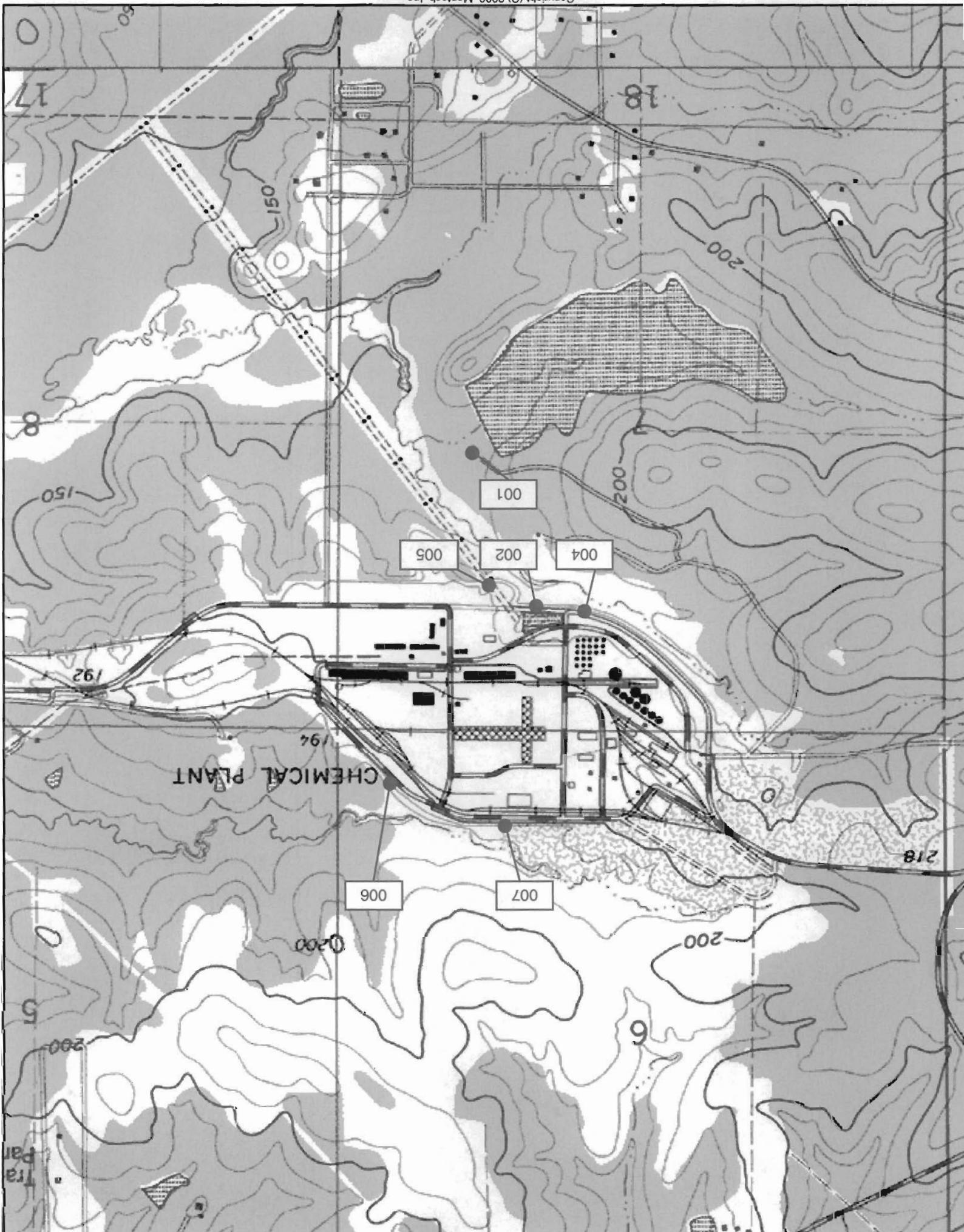
The study was performed over approximately a fifteen-month period, beginning March 2, 2005 and concluding June 17, 2006. Storm water discharges and instream flow measurements were collected during this timeframe to perform the analyses outlined in the Storm Water Flow Study Plan submitted to the ADEQ July 15, 2004.

## **4.0 Addendum**

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Site reconnaissance has determined that the background flow area for Outfalls 006 and 007 is not confined to a defined channel upstream of the facility discharges. Thus, the previously proposed background flow monitoring location is not suitable to obtain the desired information.

An alternate flow monitoring location for Outfalls 006 and 007 has been identified and is shown on the revised Figure 2. The methodology proposed for measurement of background flows at the alternate location will be to determine the total flow of the two small channels and subtract the measured flows from Outfall 006 and 007 from the totals measured at the downstream points. Evaluation of the data collected will be as proposed in the July 15, 2004 Storm Water Study Work Plan.

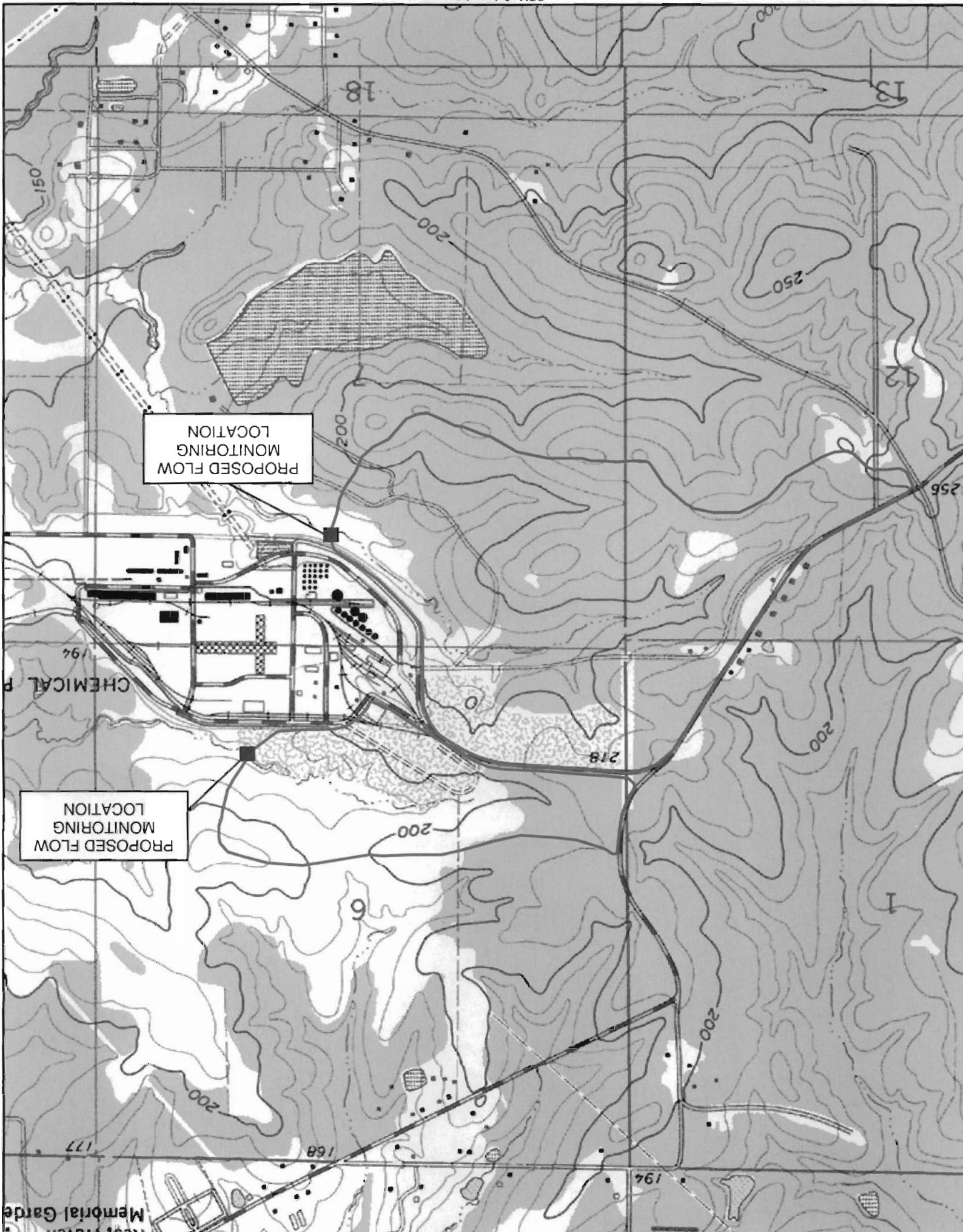


A reconnaissance survey of the site will be conducted and potential gauging stations identified in the tributary to Flat Creek north of the EDCC facility (Outfalls 006 and 007) and in the tributary south of the facility (Outfalls 002, 004, and 005) on EDCC and 007) and in the tributary south of the facility (Outfalls 002, 004, and 005) on EDCC properties (Figure 2).

Instruments will be installed at these locations to automatically record stream level at specific time intervals. The instruments will be configured to collect and log level data on a relatively short time interval in order to maximize the number of level measurements obtained during a runoff event. Periodic site visits will be made to perform maintenance, check operation, and retrieve the data from the instruments.

In-stream flow measurements will be manually collected at each gauging station by a field crew during rainfall events as part of an effort to develop a relationship between stream level and rate of flow. In-stream velocity will be measured using a Marsh-M<sup>®</sup> Birney model 201 water current meter. Measurements will be taken following a field crew during rainfall events as part of an effort to develop a relationship between stream level and rate of flow. In-stream velocity will be measured using a section area multiplied by the velocity yields the instantaneous volumetric flow for stream. This instantaneous flow rate in conjunction with the level recorded by the instruments at the time that the flow was measured will be used to develop the relationship between level and flow rate. A minimum of twelve coincident level and flow readings will be used from each gauging station to develop an independent relationship for each receiving stream upgradient of the EDCC discharges. Multiple flow measurements may be collected during a single rainfall event.

## 2.0 Hydrology Methodology



The stream level versus flow rate relationship will allow GBM<sup>c</sup> to convert the level data collected by the instruments into flow rates. The flow rates will be used to develop flow versus time hydrographs for each tributary of Flat Creek to graphically represent the rate and timing of the surface runoff from the upstream watersheds generated by the rainfall events that occurred.

The discharge from NPDEx Storm Water Outfalls 004, 005, 006, and 007 will be recorded continuously during storm events and used to generate flow versus time hydrographs for each NPDEx outfall over the duration of the study. An existing rainfall gauge will measure and record the time and amount of precipitation to correlate with flow measurements in the NPDEx storm water outfalls and receiving streams.

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### 3.0 Results/Data Analysis

The stream level versus time hydrographs for each Flat Creek tributary will be plotted together with the hydrographs for the NPDEx storm water outfalls that discharge into each respective stream for each rainfall event that occurs over the duration of the study. These plots will indicate the flow rate of surface runoff contributed by the upstream watershed and the NPDEx outfall at any given time during a specific rainfall event as well as the total volume contributed by either source over the entire event. This information will be used to evaluate the percent effluent composition of various stream flow events.

Site reconnaissance has determined that the background flow area for Outfalls 006 and 007 is not confined to a defined channel upstream of the facility discharges. Thus, the previously proposed background flow monitoring location is not suitable to obtain the desired information. An alternate flow monitoring location for Outfalls 006 and 007 has been identified and is shown on the revised Figure 2. The methodology proposed for measurement of background flows at the alternate location will be to determine the total flow of the two small channels and subtract the measured flows from Outfall 006 and 007 from the totals measured at the downstream points. Evaluation of the data collected will be as proposed in the July 15, 2004 Storm Water Study Work Plan.

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## 4.0 Addendum

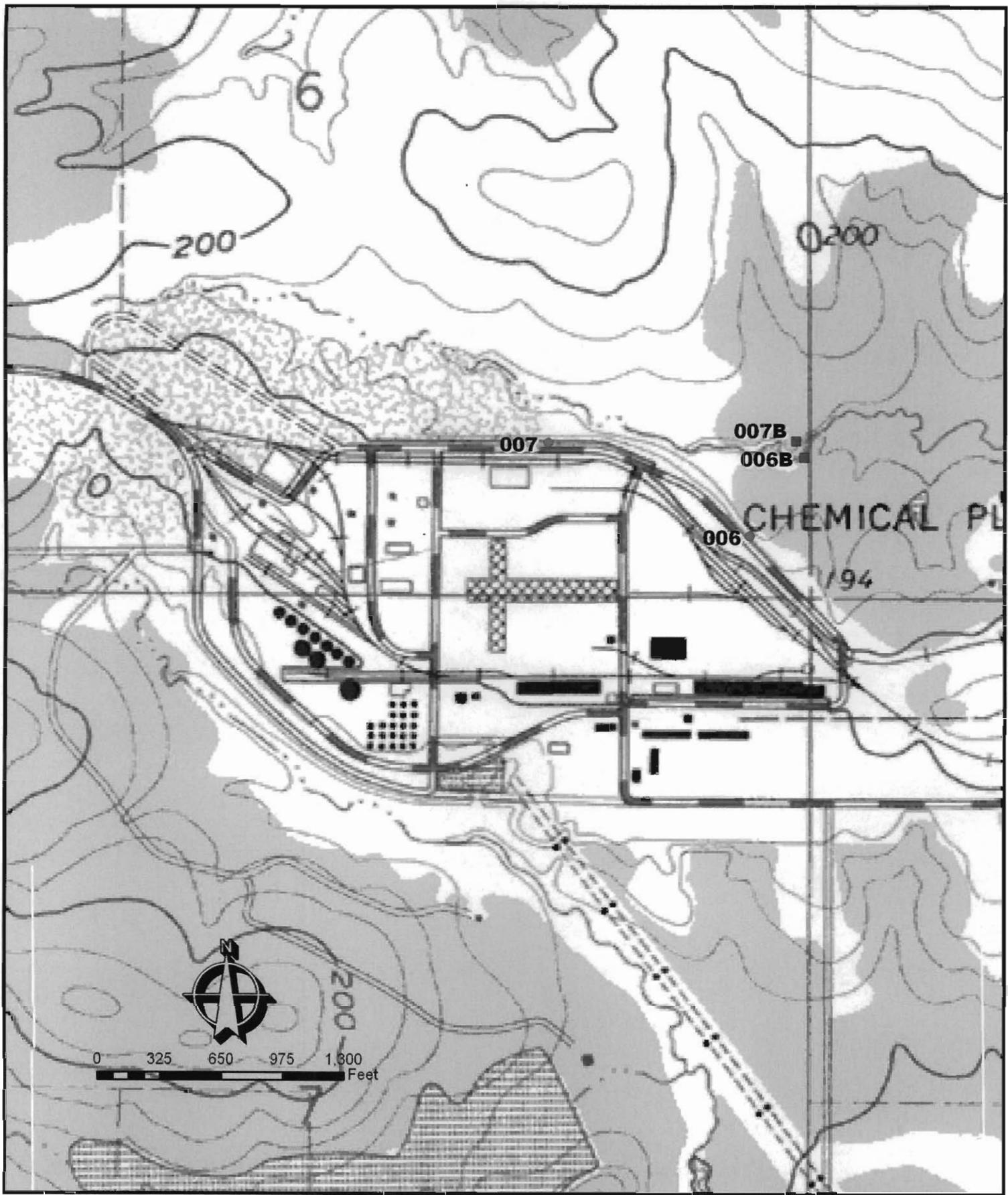


Figure 2. Map showing guaging staions 006B & 007B.

August 29, 2006

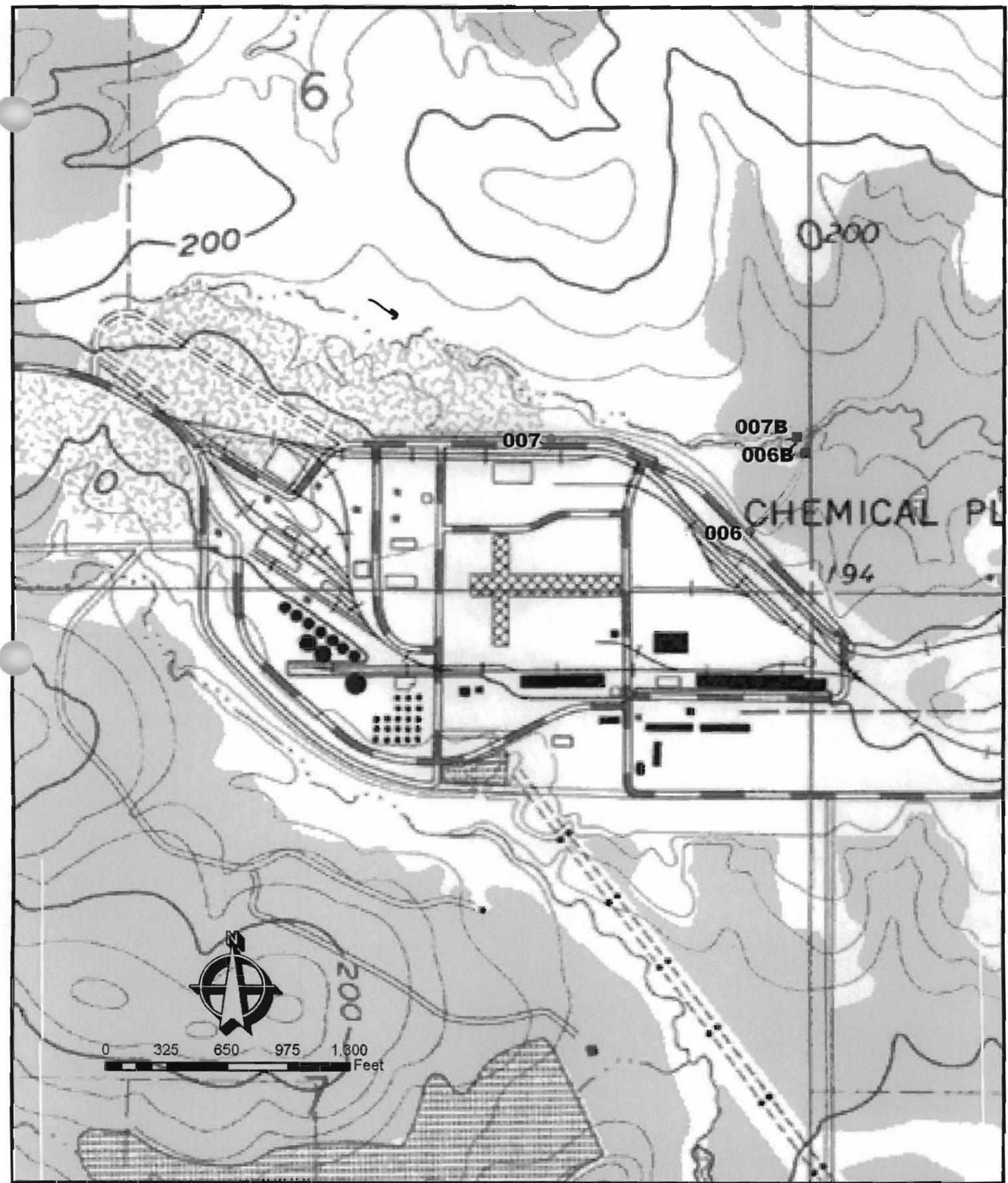


Figure 1. Map showing gauging stations.

## **3.0 Stream Level Monitoring**

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Two gauging stations were established in the north tributary on EDCC property (Figure 1) at a point where the flow in the tributary splits into two channels. One gauge was installed on each channel, tributary 006B and tributary 007B. Each gauging station was equipped with a Global Water WL-15 water level logger which was configured to record stream level at five-minute intervals. The loggers were installed at each of the gauging stations on March 2, 2005 and were removed from the EDCC facility June 17, 2006. Site visits were performed approximately every four to six weeks throughout the course of the study to retrieve the stored data from the loggers, perform necessary maintenance, minimize potential data loss due to equipment malfunction, and to ensure the loggers were operating properly. During a scheduled site visit, it was determined that the Global Water WL-15 logger installed at the background flow site designated as 006B had malfunctioned. The WL-15 logger was replaced with a HOBO® U20 level logger on February 24, 2006. The two gauging stations for the north tributary (006B and 007B) were located west of two separate road culverts which create a split stream channel but later combine a few yards downstream to convey all of the north tributary and storm water flows off of the EDCC site. Both loggers were installed in protective conduits placed on the bottom center of the main stem of the drainage channel. Precipitation data was provided by a rain gauge installed and maintained at EDCC. The rainfall data is included as Appendix B.

Instream flow measurements were manually collected at each gauging station by a field crew over a range of flow conditions (12 measurement events) to develop a relationship between stream level and rate of flow. Instream velocity was measured using a Marsh-M<sup>c</sup>Birney model 201 water current meter following protocols outlined in the GBM<sup>c</sup> & Associates Quality Assurance Plan (GBM<sup>c</sup> QAP, 2001). Flow calculations were performed using the velocity-area method. [The cross-sectional area multiplied by the velocity yields the instantaneous volumetric flow for the stream.] The field data from the flow measurements and calculations are included as Appendix C. The instantaneous flow rate was used in conjunction with the level recorded by the loggers at the time of the flow measurement to develop a relationship between water level and flow rate. Table 1 shows the date, instantaneous flow rate, and water level for each flow measurement collected at the north tributary gauges.

*Actual*

Table 1. North Tributary Flow Measurement Summary.

Date	Time	006B		007B	
		Flow (CFS)	Logger depth (ft)	Date	Time
3/2/2005	3:40 PM	0.67	0.78	3/2/2005	4:00 PM
3/29/2005	1:00 PM	0.93	0.86	3/29/2005	1:15 PM
1/23/2006	5:35 PM	0.35	0.73	1/23/2006	5:45 PM
2/24/2006	1:05 PM	0.11	0.62	2/24/2006	12:55 PM
3/20/2006	12:26 PM	4.4	1.465	3/20/2006	12:15 PM
4/25/2006	1:20 PM	0.88	0.97	4/25/2006	1:25 PM
4/29/2006	10:40 AM	1.72	1.162	4/29/2006	10:50 AM
4/29/2006	12:20 PM	2.69	1.326	4/29/2006	12:30 PM
5/4/2006	6:10 PM	3.59	1.359	5/4/2006	6:25 PM
5/4/2006	7:40 PM	2.74	1.32	5/4/2006	7:50 PM
6/17/2006	5:50 PM	1.395	1.151	6/17/2006	6:00 PM
6/17/2006	6:50 PM	0.63	1.006	6/17/2006	6:55 PM

To convert the water level measurements collected from the level loggers into a flow estimate, a rating curve was developed for each branch of north tributary based on the data in Table 1. The level versus flow data was plotted to determine the best fit curve through the data for each stream using various regression techniques. Charts showing the data and the best fit curves are included as Appendix D. It was determined that a trinomial function ( $y = a_3x^3 + a_2x^2 + a_1x + a_0$ ) yielded the best representation of the data set for the 006B tributary. The equation used to calculate flow rate for the 006B tributary:

$$y = 11.286x^3 - 28.13x^2 + 25.05x - 7.2465$$

where:  $y$  = flow rate, CFS

$x$  = water level, ft.

To represent the level to flow relationship for the 007B tributary, several regression (curve fitting) methods were assessed. A power function was found to provide the best curve fit. Therefore, the equation used to calculate flow in the 007B tributary is:

$$y = 0.0856x^{6.9528}$$

where  $y$  = flow rate, CFS

$x$  = water level, ft.

## **4.0 Outfall 006/007 Monitoring**

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7/3/04

Storm water Outfalls 006 and 007 at EDCC are equipped with prefabricated flumes for measurement of instantaneous flow rate. A 3 ft "H" flume is installed at Outfall 006, and a 4 ft "HL" flume is installed at Outfall 007. One water level recording gauge was installed on each flume. Each gauging station was equipped with a Global Water WL-15 water level logger which was configured to record water level at five-minute intervals. The loggers were installed at each of the gauging stations on March 2, 2005 and were removed from the EDCC facility June 17, 2006. Site visits were performed approximately every four to six weeks throughout the course of the study to retrieve the stored data from the loggers, perform necessary maintenance, minimize potential data loss due to equipment malfunction, and to ensure the loggers were operating properly.

Water level data recorded by the instruments was used to determine instantaneous flow rate using the flow vs. depth relationships developed by the U. S. Department of Agriculture as published in their Handbook No. 224. Flume flow tables are provided in Appendix E.

## **5.0 Findings**

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### **5.1 Background Flow vs. Outfall Flow**

Flow rates were measured and logged at storm water outfalls 006 and 007 at the EDCC facility throughout the study. The storm outfalls are situated in the headwaters of the north tributary; as discussed in the Plan (Section 4.0 addendum, 9/17/04), the background flow would be determined by simultaneously measuring total discharge of the north tributary and subtracting measured discharges from the facility. The purpose of the study was to establish the percentage volumetric contribution of plant storm water discharges to the total watershed discharge exiting EDCC property. Therefore, storm water discharge flow was totalized on an event basis and compared to the total background storm event flow in the tributary, as estimated from the rating curves, to determine a total storm event flow ratio for each event where a discharge occurred and reached the gauging stations at the property boundary.

A total of seventy-one storm discharge events were measured during the study. Flow ratios were calculated by dividing the receiving stream flow (background flow) by the discharge

flow for storm water outfalls 006 and 007. A summary of the data used in the development of the flow ratios is provided in Appendix F. Table 2 summarizes the flow rate ratios calculated from the data. Ratios are calculated and presented seasonally (summer period and seasonal period). The summer period is depicted July through October and the seasonal period as November through June.

Several statistics were calculated from the flow ratios for each season and scenario. These statistics included the mean, the median, the 25<sup>th</sup> percentile and confidence intervals about the mean at the 80%, 90% and 95% level. The 25th percentile value is the point at which 75 percent of the data set is greater than it. That is, 75% of the ratios in the data set are greater than the 25<sup>th</sup> percentile value for a given season and scenario. The median is equivalent to the 50<sup>th</sup> percentile value, such that half the data is greater than it and half the data is less than it. A confidence interval provides a statistical probability that a new set of data (ratios in this case) will result in a mean value in the range of the interval. The lower confidence interval for each probability basis is presented in Table 2 as it is the low side of the statistical range of predicted means and thus the more conservative value. Table 2 does not provide an exhaustive list of potential statistics that could be developed for regulatory use. However, the table does provide those that would be most commonly used for permitting purposes.

Table 2. Storm event flow rate ratio summary, background flow: storm effluent discharge.

Statistic	006 Seasonal	007 Seasonal	006 Summer <sup>1</sup>	007 Summer <sup>1</sup>
Lower 95% CI	53.6	15.0	0.00	0.00
Lower 90% CI	61.0	17.4	0.14	0.00
Lower 80% CI	69.5	20.1	0.53	0.00
Mean	98.7	29.4	1.7	3.5
Median	20.1	8.0	0.58	0.40
25%tile	9.2	4.0	0.42	0.31

<sup>1</sup> Zeros (0.00) appear or all statistical results less than 0.01.

## 5.2 Acute/Chronic Aquatic Toxicity

The current NPDES storm water discharge limits for Outfalls 006 and 007 at EDCC include numeric values for cadmium, lead, and zinc that are based on the presumption that 7Q10 for the receiving stream (north tributary of Flat Creek) is zero; that is, the stream is comprised of 100% storm effluent from EDCC. However, site-specific data has shown that using the lower 95% confidence interval (53.6:1 Outfall 006, 15:1 Outfall 007) during the seasonal (November – June) period, the tributary contains only 8.53% storm effluent associated with industrial activity at EDCC. Cadmium, lead and zinc analytical data collected for the

NPDES Permit application was used in a reasonable potential screen to determine the minimum background to source flow ratio required to prevent instream acute and chronic aquatic toxicity in the north tributary to Flat Creek. The screen results are shown in Table 3.

Table 3. Acute/Chronic Aquatic Toxicity Screen Results, EDCC Outfalls 006/007.

Background to Source ratio (B:S)			
Outfall (95% CI)	Cadmium	Lead	Zinc
006 (53.6)	7.13	201.77	215.2
007 (15.0)	0.26	13.03	9.92

### 5.3 Total Dissolved Solids

The current NPDES Permit includes effluent limits for Total Dissolved Solids (TDS) for Outfalls 006 and 007 based on limited instantaneous flow data for the storm water outfalls available at the time the application was prepared. As a result of this study, seasonal period storm water effluent flows as a ratio of background flow were determined and may be used instead of the assumed 4 CFS background flow used in the water quality standard implementation process in the following formula:

$$C_e Q_e + C_b Q_b \leq C_{wqs} (Q_e + Q_b)$$

where:  $C_e$  = effluent concentration, mg/l

$Q_e$  = effluent flow, CFS

$C_b$  = background concentration, 67 mg/l

$Q_b$  = background flow, CFS

$C_{wqs}$  = Water Quality Standard concentration, 123 mg/l.

Substituting the seasonal period 95% CI background to source flow ratio for Outfalls 006 and 007 results in the appropriate TDS limit derivations shown in Table 4.

Table 4. TDS Limit Derivation, EDCC Outfalls 006/007.

Outfall (95% CI)	Seasonal TDS Monthly Ave Limit (mg/l)
006 (53.6)	3124.6
007 (15.0)	963.0

## **6.0 Recommendations**

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The EDCC Storm Water Flow Study has successfully demonstrated that background flow occurs in the north tributary to Flat Creek during storm water discharge events seasonally, and that statistically conservative analysis of the ratio of background to source flows indicates that the current NPDES Permit limits for certain parameters are not appropriate during the November through June period. Thus, our recommendations are:

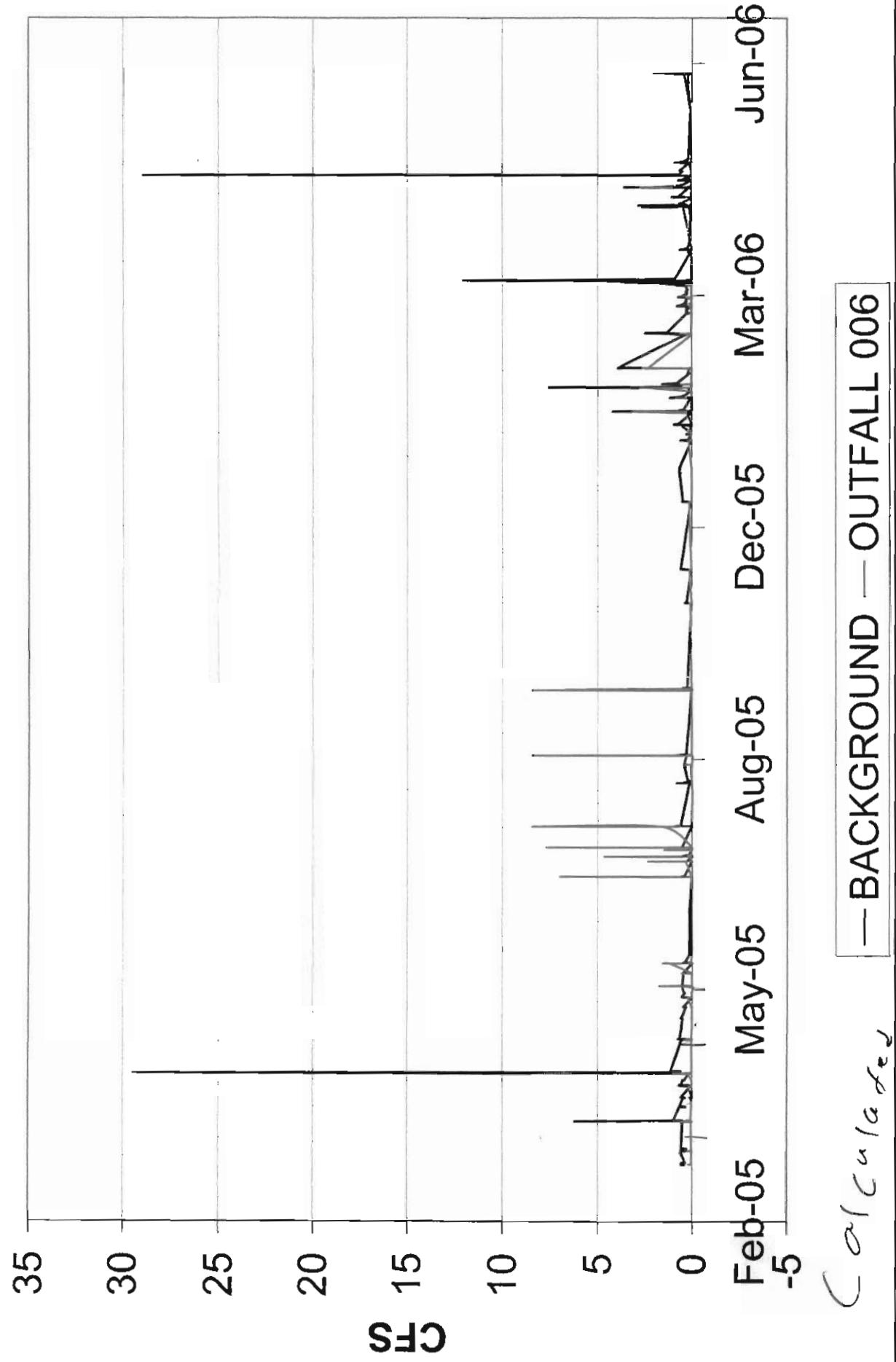
1. *Eliminate all effluent limits for cadmium at Outfall 006 using the 95% CI ratio of background-to-source for the period November through June. Current limits to remain for July – October.*
2. *Revise the monthly average/daily maximum effluent limits for lead at Outfall 006 to 139.1/279.0 ug/l using the 95% CI ratio of background-to-source for the period November through June. Current limits to remain for July – October.*
3. *Revise the monthly average/daily maximum effluent limits for zinc at Outfall 006 to 2,198.1/4,409.9 ug/l using the 95% CI ratio of background-to-source for the period November through June. Current limits to remain for July – October.*
4. *Revise the monthly average/daily maximum effluent limits for TDS at Outfall 006 to 3,124/4,686 mg/l using the 95% CI ratio of background-to-source for the period November through June. Current limits to remain for July – October.*
5. *Eliminate all effluent limits for cadmium, lead and zinc at Outfall 007 using the 95% CI ratio of background-to-source for the period November through June. Current limits to remain for July – October.*
6. *Revise the monthly average/daily maximum effluent limits for TDS at Outfall 007 to 963/1,444 mg/l using the 95% CI ratio of background-to-source for the period November through June. Current limits to remain for July – October.*
7. *Revise the critical dilution and dilution series for Acute Biomonitoring at Outfall 006 using the 95% CI ratio of background-to-source for the period November through June. Current dilutions to remain for July – October.*
8. *Revise the critical dilution and dilution series for Acute Biomonitoring at Outfall 006 using the 95% CI ratio of background-to-source for the period November through June. Current dilutions to remain for July – October.*

**Appendix A**

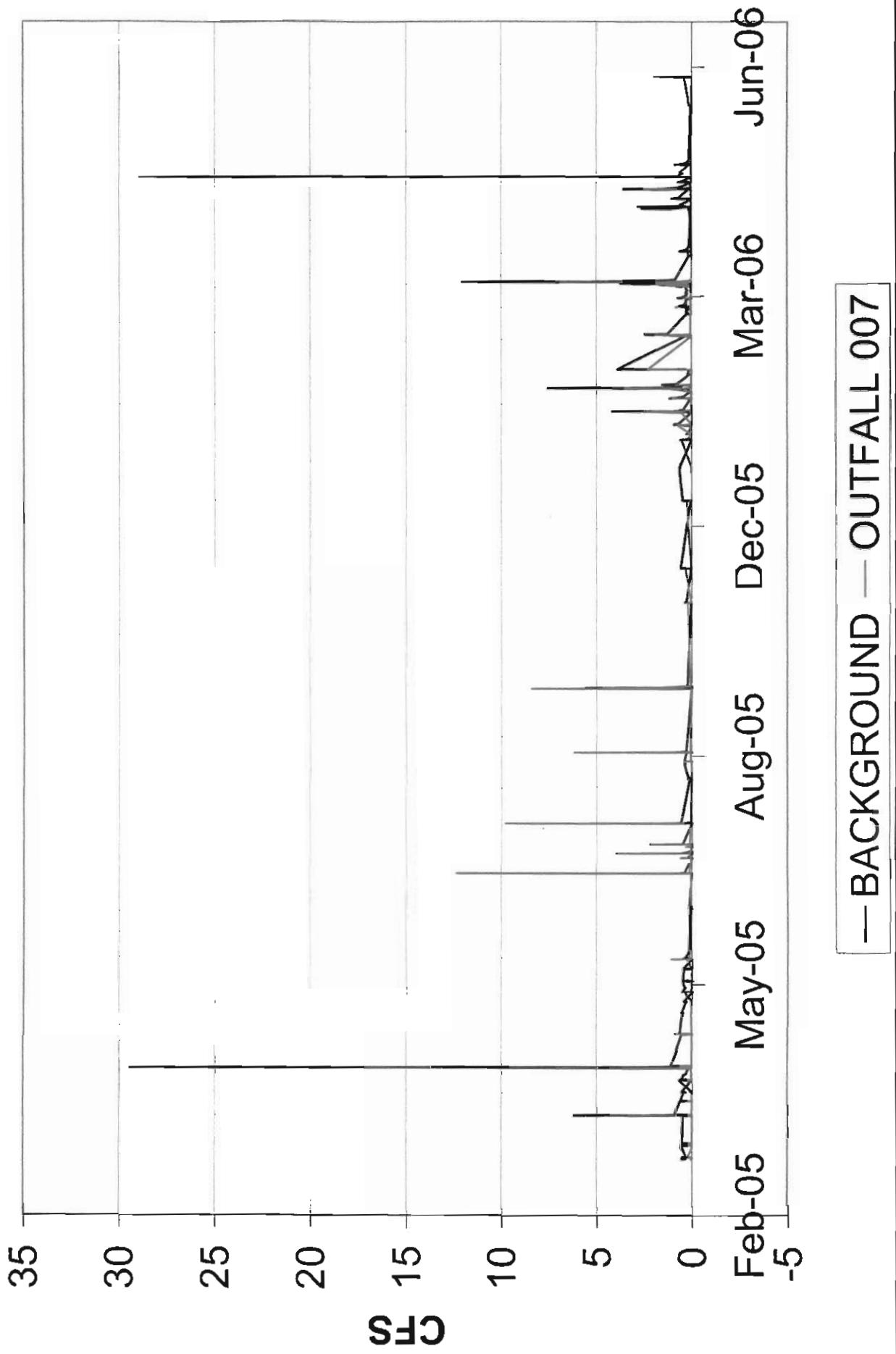
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**Recorded Water Levels and Flow Data**

## EDCC-INSTANTANEOUS FLOW



## EDCC-INSTANTANEOUS FLOW



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**Appendix B**

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**Rainfall Data**

## EOCC Rainfall Data

2005	Rainfall Inches
Date	
1-Jan	
2-Jan	
3-Jan	0.2
4-Jan	0
5-Jan	0
6-Jan	0.33
7-Jan	1
8-Jan	
9-Jan	
10-Jan	0.5
11-Jan	0
12-Jan	0
13-Jan	1.05
14-Jan	0
15-Jan	
16-Jan	
17-Jan	0
18-Jan	0
19-Jan	0
20-Jan	0
21-Jan	0
22-Jan	
23-Jan	
24-Jan	0
25-Jan	0
26-Jan	0
27-Jan	0
28-Jan	0.23
29-Jan	
30-Jan	
31-Jan	1.18
1-Feb	0.07
2-Feb	0.53
3-Feb	0
4-Feb	0
5-Feb	
6-Feb	
7-Feb	0.51
8-Feb	0.3
9-Feb	0
10-Feb	0
11-Feb	0
12-Feb	
13-Feb	
14-Feb	0.03
15-Feb	0
16-Feb	0
17-Feb	0
18-Feb	0
19-Feb	
20-Feb	
21-Feb	0.3
22-Feb	0
23-Feb	0
24-Feb	0.58
25-Feb	0.03
26-Feb	
27-Feb	
28-Feb	0.07
1-Mar	0
2-Mar	0
3-Mar	0.2
4-Mar	0
5-Mar	
6-Mar	
7-Mar	0
8-Mar	0.13
9-Mar	0.07
10-Mar	0.1
11-Mar	0
12-Mar	
13-Mar	
14-Mar	0
15-Mar	0
16-Mar	0
17-Mar	0
18-Mar	0
19-Mar	
20-Mar	
21-Mar	0.05
22-Mar	0.72
23-Mar	0
24-Mar	0
25-Mar	
26-Mar	
27-Mar	
28-Mar	0.36
29-Mar	0
30-Mar	0
31-Mar	0
1-Apr	0.13
2-Apr	
3-Apr	
4-Apr	0
5-Apr	0
6-Apr	0.36
7-Apr	0.07

2005	Rainfall Inches
8-Apr	0.1
9-Apr	
10-Apr	
11-Apr	2
12-Apr	2.07
13-Apr	0
14-Apr	0
15-Apr	0
16-Apr	
17-Apr	
18-Apr	0
19-Apr	0
20-Apr	0
21-Apr	0
22-Apr	0
23-Apr	
24-Apr	
25-Apr	0
26-Apr	0.54
27-Apr	0
28-Apr	0
29-Apr	0
30-Apr	
1-May	
2-May	0.07
3-May	0
4-May	0
5-May	0
6-May	0
7-May	
8-May	
9-May	0.13
10-May	0
11-May	0
12-May	0
13-May	0
14-May	
15-May	
16-May	0.3
17-May	0
18-May	0
19-May	0
20-May	0
21-May	
22-May	
23-May	0
24-May	0
25-May	0.26
26-May	0
27-May	0
28-May	
29-May	
30-May	
31-May	0.56
1-Jun	0
2-Jun	0.03
3-Jun	0
4-Jun	
5-Jun	
6-Jun	0
7-Jun	0
8-Jun	0.1
9-Jun	0
10-Jun	0
11-Jun	
12-Jun	
13-Jun	0
14-Jun	0
15-Jun	0
16-Jun	0
17-Jun	0
18-Jun	
19-Jun	
20-Jun	0.28
21-Jun	0
22-Jun	0
23-Jun	0
24-Jun	0
25-Jun	
26-Jun	
27-Jun	0
28-Jun	0
29-Jun	0
30-Jun	0
1-Jul	0
2-Jul	
3-Jul	
4-Jul	
5-Jul	0
6-Jul	1.04
7-Jul	0
8-Jul	0
9-Jul	
10-Jul	
11-Jul	0
12-Jul	0
13-Jul	0.23
14-Jul	

2005	Rainfall Inches
15-Jul	1.2
16-Jul	
17-Jul	
18-Jul	0.15
19-Jul	0.41
20-Jul	0
21-Jul	0
22-Jul	0
23-Jul	
24-Jul	
25-Jul	0
26-Jul	0
27-Jul	0
28-Jul	1.12
29-Jul	0
30-Jul	
31-Jul	
1-Aug	0
2-Aug	0
3-Aug	0
4-Aug	0
5-Aug	0
6-Aug	
7-Aug	
8-Aug	0
9-Aug	0
10-Aug	0
11-Aug	0
12-Aug	0
13-Aug	
14-Aug	
15-Aug	0.13
16-Aug	0.2
17-Aug	0
18-Aug	0
19-Aug	0
20-Aug	
21-Aug	
22-Aug	0.22
23-Aug	0
24-Aug	0.38
25-Aug	0
26-Aug	0
27-Aug	
28-Aug	
29-Aug	1.04
30-Aug	0
31-Aug	0
1-Sep	0
2-Sep	0
3-Sep	
4-Sep	
5-Sep	
6-Sep	0
7-Sep	0
8-Sep	0
9-Sep	0
10-Sep	
11-Sep	
12-Sep	0
13-Sep	0
14-Sep	0
15-Sep	0
16-Sep	0.16
17-Sep	
18-Sep	
19-Sep	0
20-Sep	0
21-Sep	0
22-Sep	0
23-Sep	0
24-Sep	
25-Sep	
26-Sep	2
27-Sep	0
28-Sep	0
29-Sep	0.03
30-Sep	0
1-Oct	
2-Oct	
3-Oct	0
4-Oct	0
5-Oct	0
6-Oct	0
7-Oct	0
8-Oct	
9-Oct	
10-Oct	
11-Oct	0
12-Oct	0
13-Oct	0
14-Oct	0
15-Oct	
16-Oct	
17-Oct	0
18-Oct	0
19-Oct	0
20-Oct	0

Draught from  
outfall  
in  
DMF

EDCC Rainfall Data

2005	Rainfall Inches
21-Oct	0
22-Oct	
23-Oct	
24-Oct	0
25-Oct	0
26-Oct	0
27-Oct	0
28-Oct	0
29-Oct	
30-Oct	
31-Oct	0
1-Nov	0.66
2-Nov	0
3-Nov	0
4-Nov	0
5-Nov	
6-Nov	
7-Nov	0
8-Nov	0
9-Nov	0
10-Nov	0
11-Nov	0
12-Nov	
13-Nov	
14-Nov	0.26
15-Nov	0.13
16-Nov	0.33
17-Nov	0
18-Nov	0
19-Nov	
20-Nov	
21-Nov	0.07
22-Nov	0
23-Nov	0
24-Nov	
25-Nov	
26-Nov	
27-Nov	
28-Nov	0.49
29-Nov	0
30-Nov	0
1-Dec	0
2-Dec	0
3-Dec	
4-Dec	0.5
5-Dec	0
6-Dec	0
7-Dec	0
8-Dec	1.25
9-Dec	0
10-Dec	
11-Dec	
12-Dec	0
13-Dec	0
14-Dec	0.02
15-Dec	0.5
16-Dec	0
17-Dec	
18-Dec	
19-Dec	0
20-Dec	0
21-Dec	0
22-Dec	0
23-Dec	
24-Dec	
25-Dec	
26-Dec	
27-Dec	0
28-Dec	0
29-Dec	0
30-Dec	0
31-Dec	
2006	
1-Jan	
2-Jan	
3-Jan	0
4-Jan	0
5-Jan	0
6-Jan	0
7-Jan	
8-Jan	
9-Jan	0
10-Jan	0.6
11-Jan	0.07
12-Jan	0
13-Jan	0.18
14-Jan	
15-Jan	
16-Jan	0
17-Jan	0.72
18-Jan	0
19-Jan	0
20-Jan	0
21-Jan	
22-Jan	
23-Jan	2
24-Jan	0
25-Jan	0

2006	Rainfall Inches
26-Jan	0
27-Jan	0
28-Jan	
29-Jan	
30-Jan	0.35
31-Jan	0
1-Feb	0
2-Feb	0.8
3-Feb	0
4-Feb	
5-Feb	
6-Feb	0.25
7-Feb	0
8-Feb	0
9-Feb	0
10-Feb	0
11-Feb	
12-Feb	
13-Feb	
14-Feb	
15-Feb	
16-Feb	
17-Feb	
18-Feb	
19-Feb	
20-Feb	
21-Feb	
22-Feb	
23-Feb	
24-Feb	
25-Feb	
26-Feb	
27-Feb	1.25
28-Feb	0
1-Mar	0
2-Mar	0
3-Mar	0
4-Mar	
5-Mar	
6-Mar	0.1
7-Mar	0
8-Mar	0
9-Mar	0
10-Mar	0.4
11-Mar	
12-Mar	
13-Mar	0
14-Mar	0.23
15-Mar	0
16-Mar	0
17-Mar	0
18-Mar	
19-Mar	
20-Mar	2
21-Mar	0.37
22-Mar	0
23-Mar	0
24-Mar	0
25-Mar	0
26-Mar	
27-Mar	0
28-Mar	0
29-Mar	0
30-Mar	0
31-Mar	0
1-Apr	
2-Apr	
3-Apr	0.3
4-Apr	0
5-Apr	0
6-Apr	0
7-Apr	0
8-Apr	
9-Apr	
10-Apr	0
11-Apr	0
12-Apr	0
13-Apr	0
14-Apr	0
15-Apr	
16-Apr	
17-Apr	0
18-Apr	0
19-Apr	0
20-Apr	0
21-Apr	0.8
22-Apr	
23-Apr	
24-Apr	0.65
25-Apr	0
26-Apr	0.45
27-Apr	0
28-Apr	0
29-Apr	
30-Apr	
1-May	1
2-May	0
3-May	0.3

2006	Rainfall Inches
4-May	0
5-May	1
6-May	
7-May	
8-May	0.2
9-May	0.1
10-May	0.3
11-May	0
12-May	
13-May	
14-May	
15-May	0
16-May	0
17-May	0
18-May	0
19-May	0
20-May	

2006	Rainfall Inches
6-Jun	0
7-Jun	1.1
8-Jun	0
9-Jun	0
10-Jun	
11-Jun	
12-Jun	0
13-Jun	0
14-Jun	0
15-Jun	0
16-Jun	0
17-Jun	

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**Appendix C**

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**Flow Measurement Data Collected in the Field**

form?

El Dorado Chemical

date

3/2/2005

Start  
Stop

1550  
1600

3:45

0:50

Station: 086b EDCC

Waterbody Trib

Crew: BJP / JJF

Level

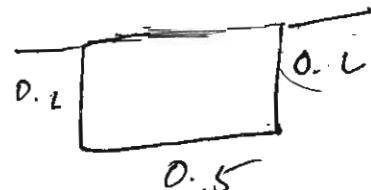
0.78 logger

GPS

Width (ft):	3	Area:	0.65	Max Vel:	1.24	
Flow (cfs):	0.67	Velocity:	0.90	Min Vel:	0	

N

Distance from initial point (ft)	1	2	Avg. velocity at point (ft/sec)	4	5	6	7	Average Discharge (cfs)
0.5	0.5	0.2	1.24	0.1	0.124	0.6	0.12	
1	0.5	0.2	1.22	0.1	0.122	0.6	0.12	
1.5	0.5	0.4	1.24	0.2	0.248	0.6	0.25	
2	0.5	0.2	0.98	0.1	0.098	0.6	0.10	
2.5	0.5	0.2	0.73	0.1	0.073	0.6	0.07	
3	0.5	0.1	0	0.05	0	0.6	0.00	
				0	0	0.6	0.00	
				0	0	0.6	0.00	
				0	0	0.6	0.00	
				0	0	0.6	0.00	
total	3	1.3	5.41	0.65			0.665	
average	0.5	0.216667	0.901667	0.065			0.073889	



$$0.65 \times 0.9 = 0.585?$$

W = 3 ft

El Dorado Chemical

date

3/29/2005

Start

1300

Stop

1315

Level



Station: 006b EDCC

Waterbody Trib

Crew: AAS / JJF

Width (ft): 3.5	Area: 1.0395	Max Vel: 1.7
Flow (cfs): 0.93	Velocity: 0.70	Min Vel: 0

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.35	0.35	0.2	0.17	0.07	0.0119	0.6	0.01
0.7	0.35	0.3	1.2	0.105	0.126	0.6	0.13
1.05	0.35	0.32	1.3	0.112	0.1456	0.6	0.15
1.4	0.35	0.35	1.7	0.1225	0.20825	0.6	0.21
1.75	0.35	0.45	1.5	0.1575	0.23625	0.6	0.24
2.1	0.35	0.5	0.8	0.175	0.14	0.6	0.14
2.45	0.35	0.5	0.35	0.175	0.06125	0.6	0.06
2.8	0.35	0.25	0	0.0875	0	0.6	0.00
3.15	0.35	0.1	0	0.035	0	0.6	0.00
3.5	0.35	0	0	0	0	0.6	0.00
total	3.15	2.97	7.02	1.0395			0.929
average	0.35	0.297	0.702	0.10395			0.10325

El Dorado Chemical	date	3/29/2005	Start	1315
Station: 007b EDCC			Stop	1320
Waterbody Trib			Level	0.86
Crew: AAS / JJF				
Width (ft):	Area:	1.57	Max Vel:	
Flow (cfs):	0.05	Velocity:	0.03	Min Vel:

$$A = ((\theta - \sin\theta)D^2)/8$$

for  $y < D/2 \quad \theta = \pi - 2\sin^{-1} [1-(2y/D)]$   
 for  $y > D/2 \quad \theta = \pi + 2\sin^{-1} [(2y/D) - 1]$

Station 007b EDCC flows through a 24" diameter pipe at low velocity  
 The following calculations are partially full round cross sections (Page 363, Mott).

$$A = ((\theta - \sin\theta)D^2)/8$$

for  $y < D/2 \quad \theta = \pi - 2\sin^{-1} [1-(2y/D)]$   
 for  $y > D/2 \quad \theta = \pi + 2\sin^{-1} [(2y/D) - 1]$

$$\begin{aligned} D &= 2 \text{ ft} \\ y &= 1 \text{ ft} \\ v &= 0.03 \text{ ft/s} \\ \theta &= 3.14 \text{ radians} \\ A &= 1.57 \text{ ft}^2 \\ Q &= 0.047 \text{ CFS} \end{aligned}$$

El Dorado Chemical

date

1/23/2006

Start

1735

Stop

1742

Station:	006b EDCC			Level	
Waterbody Trib					
Crew:	SKH / JJF				
Width (ft):	4.5	Area:	1.6		
Flow (cfs):	0.35	Velocity:	0.16	Min Vel: 0	

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.2	0.05	0.1	0.005	0.6	0.01
1	0.5	0.3	0.3	0.15	0.045	0.6	0.05
1.5	0.5	0.5	0.33	0.25	0.0825	0.6	0.08
2	0.5	0.6	0.14	0.3	0.042	0.6	0.04
2.5	0.5	0.6	0.35	0.3	0.105	0.6	0.11
3	0.5	0.5	0.26	0.25	0.065	0.6	0.07
3.5	0.5	0.4	0.04	0.2	0.008	0.6	0.01
4	0.5	0.1	0	0.05	0	0.6	0.00
4.5	0.5	0	0	0	0	0.6	0.00
total	4.5	3.2	1.47	1.6			0.353
average	0.5	0.355556	0.163333	0.177778			0.039167



El Dorado Chemical

date

1/23/2006

Start

1745

Stop

1750

Station:	007b EDCC		
Waterbody Trib			
Crew:	SKH / JJF		
Width (ft):	3	Area:	0.6
Flow (cfs):	0.40	Velocity:	0.66
		Max Vel:	0.95
		Min Vel:	0.51

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.1	0.63	0.05	0.0315	0.6	0.03
1	0.5	0.2	0.51	0.1	0.051	0.6	0.05
1.5	0.5	0.2	0.65	0.1	0.065	0.6	0.07
2	0.5	0.3	0.69	0.15	0.1035	0.6	0.10
2.5	0.5	0.2	0.95	0.1	0.095	0.6	0.10
3	0.5	0.2	0.55	0.1	0.055	0.6	0.06
total	3	1.2	3.98	0.6			0.401
average	0.5	0.2	0.663333	0.1			0.066833

El Dorado Chemical

date

2/24/2006

Start

1305

Stop

1310

Station:	006b EDCC		
Waterbody	Trib		
Crew:	SKH / JJF		
Width (ft):	2.8	Area:	0.25
Flow (cfs):	0.11	Velocity:	0.38
		Max Vel:	0.15
		Min Vel:	0

Level

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.1	0.7	0.05	0.035	0.6	0.04
1	0.5	0.1	0.15	0.05	0.0075	0.6	0.01
1.5	0.5	0.1	0.7	0.05	0.035	0.6	0.04
2	0.5	0.1	0.7	0.05	0.035	0.6	0.04
2.5	0.5	0.1	0	0.05	0	0.6	0.00
2.8	0.3	0	0	0	0	0.6	0.00
total	2.8	0.5	2.25	0.25			0.113
average	0.466667	0.083333	0.375	0.041667			0.01875

El Dorado Chemical

date

2/24/2006

Start

1255

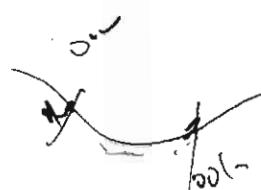
Stop

1300

Station:	007b EDCC		Level	
Waterbody Trib				
Crew:	SKH / JJF			
Width (ft):	3.8	Area: 0.55		
Flow (cfs):	-0.09	Velocity: 0.03	Min Vel: 0	

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.1	0	0.05	0	0.6	0.00
1	0.5	0.2	0.01	0.1	0.001	0.6	0.00
1.5	0.5	0.2	0.01	0.1	0.001	0.6	0.00
2	0.5	0.2	0.05	0.1	0.005	0.6	0.01
2.5	0.5	0.2	0.1	0.1	0.01	0.6	0.01
3	0.5	0.2	0.02	0.1	0.002	0.6	0.00
3.8	0.8	0	0	0	0	0.6	0.00
total	3.8	1.1	0.19	0.55			-0.094
average	0.542857	0.157143	0.027143	0.078571			0.002714

note: measured flow with 006b flow. Subtracted 006b(0.113) from 007b total cfs(0.019)



El Dorado Chemical

date

3/2/2005

Start

1600

Stop

1610

Station: 007b EDCC					
Waterbody Trib				Level	0.86
Crew: BJP / JJF					
Width (ft): 2	Area: 0.45	Max Vel: 0.05			
Flow (cfs): 0.02	Velocity: 0.03	Min Vel: 0			

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.2	0.02	0.1	0.002	0.6	0.00
1	0.5	0.4	0.05	0.2	0.01	0.6	0.01
1.5	0.5	0.2	0.05	0.1	0.005	0.6	0.01
2	0.5	0.1	0	0.05	0	0.6	0.00
total	2	0.9	0.12	0.45			0.017
average	0.5	0.225	0.03	0.1125			0.00425

El Dorado Chemical

date

3/20/2006

Start

1215

Stop

1220

Station:	007b EDCC		
Waterbody Trib			
Crew:	SKH / JJF		
Width (ft):	9	Area:	6.4
Flow (cfs):	10.32	Velocity:	2.07

Level

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
1	1	0.2	0.59	0.2	0.118	0.6	0.12
2	1	0.4	2.19	0.4	0.876	0.6	0.88
3	1	0.6	2.75	0.6	1.65	0.6	1.65
4	1	0.9	3.37	0.9	3.033	0.6	3.03
5	1	0.9	3.29	0.9	2.961	0.6	2.96
6	1	1	2.7	1	2.7	0.6	2.70
7	1	1	2.55	1	2.55	0.6	2.55
8	1	0.7	0.94	0.7	0.658	0.6	0.66
9	1	0.7	0.25	0.7	0.175	0.6	0.18
<b>total</b>	<b>9</b>	<b>6.4</b>	<b>18.63</b>	<b>6.4</b>			<b>10.323</b>
<b>average</b>	<b>1</b>	<b>0.711111</b>	<b>2.07</b>	<b>0.711111</b>			<b>1.635667</b>

14.72

note: measured flow with 006b flow. Subtracted 006b(4.398) from 007b total cfs(14.721)

El Dorado Chemical

date

3/20/2006

Start

1226

Stop

1231

Station:	006b EDCC		
Waterbody Trib			
Crew:	SKH / JJF		
Width (ft):	5.3	Area:	2.6
Flow (cfs):	4.40	Velocity:	1.18
		Max Vel:	2.86
		Min Vel:	0

Level

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.2	0	0.1	0	0.6	0.00
1	0.5	0.3	0.33	0.15	0.0495	0.6	0.05
1.5	0.5	0.5	1.31	0.25	0.3275	0.6	0.33
2	0.5	0.7	2.08	0.35	0.728	0.6	0.73
2.5	0.5	0.8	2.86	0.4	1.144	0.6	1.14
3	0.5	0.7	2.16	0.35	0.756	0.6	0.76
3.5	0.5	0.7	1.73	0.35	0.6055	0.6	0.61
4	0.5	0.7	1.5	0.35	0.525	0.6	0.53
4.5	0.5	0.5	1.05	0.25	0.2625	0.6	0.26
5	0.5	0.1	0	0.05	0	0.6	0.00
5.3	0.3	0	0	0	0	0.6	0.00
<b>total</b>	<b>4.5</b>	<b>5.2</b>	<b>13.02</b>	<b>2.6</b>			<b>4.398</b>
<b>average</b>	<b>0.5</b>	<b>0.472727</b>	<b>1.183636</b>	<b>0.236364</b>			<b>0.488667</b>

El Dorado Chemical

date

4/25/2006

Start

1320

Stop

1330

Station:	006b EDCC						
Waterbody Trib							Level
Crew:	SKH / JJF						
Width (ft):	3.7	Area:	0.85	Max Vel:	1.45		
Flow (cfs):	0.88	Velocity:	1.00	Min Vel:	0.51		

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0	0	0.2	0.47	0	0	0.6	0.00
0.5	0.5	0.2	0.72	0.1	0.072	0.6	0.07
1	0.5	0.3	0.93	0.15	0.1395	0.6	0.14
1.5	0.5	0.3	1.21	0.15	0.1815	0.6	0.18
2	0.5	0.3	1.45	0.15	0.2175	0.6	0.22
2.5	0.5	0.2	1.05	0.1	0.105	0.6	0.11
3	0.5	0.2	1.15	0.1	0.115	0.6	0.12
3.5	0.5	0.2	0.51	0.1	0.051	0.6	0.05
<b>total</b>	<b>3.5</b>	<b>1.7</b>	<b>7.02</b>	<b>0.85</b>			<b>0.882</b>
<b>average</b>	<b>0.5</b>	<b>0.242857</b>	<b>1.002857</b>	<b>0.121429</b>			<b>0.125929</b>

El Dorado Chemical

date

4/29/2006

Start

1220

Stop

1225

Station:	006b EDCC						
Waterbody Trib						Level	1.2 staff
Crew:	BJP / JB						
Width (ft):	4.5	Area:	1.75	Max Vel:	2.2		
Flow (cfs):	2.69	Velocity:	1.31	Min Vel:	0		

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.4	1	0.2	0.2	0.6	0.20
1	0.5	0.5	1.73	0.25	0.4325	0.6	0.43
1.5	0.5	0.5	2.2	0.25	0.55	0.6	0.55
2	0.5	0.5	2.1	0.25	0.525	0.6	0.53
2.5	0.5	0.5	1.6	0.25	0.4	0.6	0.40
3	0.5	0.5	1.46	0.25	0.365	0.6	0.37
3.5	0.5	0.3	1.05	0.15	0.1575	0.6	0.16
4	0.5	0.2	0.61	0.1	0.061	0.6	0.06
4.5	0.5	0.1	0	0.05	0	0.6	0.00
total	4.5	3.5	11.75	1.75			2.691
average	0.5	0.388889	1.305556	0.194444			0.299

El Dorado Chemical

date

4/29/2006

Start

1040

Stop

1045

Station:	006b EDCC			Level	1.05 staff gage		
Waterbody Trib							
Crew:	BJP / JB						
Width (ft):	4	Area:	1.3				
/Flow (cfs):	1.72	Velocity:	1.17	Max Vel: 1.87 Min Vel: 0.4			

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.3	0.4	0.15	0.06	0.6	0.06
1	0.5	0.4	1.55	0.2	0.31	0.6	0.31
1.5	0.5	0.4	1.87	0.2	0.374	0.6	0.37
2	0.5	0.5	1.77	0.25	0.4425	0.6	0.44
2.5	0.5	0.4	1.32	0.2	0.264	0.6	0.26
3	0.5	0.3	1.05	0.15	0.1575	0.6	0.16
3.5	0.5	0.2	0.73	0.1	0.073	0.6	0.07
4	0.5	0.1	0.7	0.05	0.035	0.6	0.04
<b>total</b>	<b>4</b>	<b>2.6</b>	<b>9.39</b>	<b>1.3</b>			<b>1.716</b>
<b>average</b>	<b>0.5</b>	<b>0.325</b>	<b>1.17375</b>	<b>0.1625</b>			<b>0.2145</b>

El Dorado Chemical date 4/29/2006 Start 1050  
Stop 1055

Station:	007b EDCC					
Waterbody Trib					Level	0.65
Crew:	BJP / JB					
Width (ft):	4.5	Area:	1.3	Max Vel:	1.47	
Flow (cfs):	1.70	Velocity:	1.16	Min Vel:	0	

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.3	1.23	0.15	0.1845	0.6	0.18
1	0.5	0.3	1.39	0.15	0.2085	0.6	0.21
1.5	0.5	0.4	1.46	0.2	0.292	0.6	0.29
2	0.5	0.4	1.35	0.2	0.27	0.6	0.27
2.5	0.5	0.4	1.47	0.2	0.294	0.6	0.29
3	0.5	0.3	1.35	0.15	0.2025	0.6	0.20
3.5	0.5	0.3	1.34	0.15	0.201	0.6	0.20
4	0.5	0.1	0.86	0.05	0.043	0.6	0.04
4.5	0.5	0.1	0	0.05	0	0.6	0.00
total	4.5	2.6	10.45	1.3			1.696
average	0.5	0.288889	1.161111	0.144444			0.188389

flow is a combination of 006b and 007b

$$007b = (007b + 006b) - 006b$$

$$007b = -0.020$$

$$007b = 0$$

El Dorado Chemical	date	4/29/2006	Start	1230
			Stop	1235
Station: 007b EDCC				
Waterbody Trib			Level	0.65
Crew: BJP / JB				
Width (ft): 5	Area: 1.85	Max Vel: 1.74		
Flow (cfs): 2.52	Velocity: 1.13	Min Vel: 0		

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.1	0	0.05	0	0.6	0.00
1	0.5	0.3	1.05	0.15	0.1575	0.6	0.16
1.5	0.5	0.4	1.51	0.2	0.302	0.6	0.30
2	0.5	0.5	1.74	0.25	0.435	0.6	0.44
2.5	0.5	0.5	1.6	0.25	0.4	0.6	0.40
3	0.5	0.5	1.58	0.25	0.395	0.6	0.40
3.5	0.5	0.5	1.44	0.25	0.36	0.6	0.36
4	0.5	0.4	1.35	0.2	0.27	0.6	0.27
4.5	0.5	0.4	1.01	0.2	0.202	0.6	0.20
5	0.5	0.1	0	0.05	0	0.6	0.00
<hr/>							
total	4.5	3.7	11.28	1.85			2.522
average	0.5	0.37	1.128	0.185			0.280167

flow is a combination of 006b and 007b

$$007b = (007b + 006b) - 006b$$

$$007b = -0.170$$

$$007b = 0$$

El Dorado Chemical	date	5/4/2006	Start	1950
			Stop	2000
Station: 007b EDCC				
Waterbody Trib			Level	1.7 at logger
Crew: JBB/JJF				
Width (ft): 6	Area: 3.55	Max Vel: 2.4		
Flow (cfs): 4.21	Velocity: 1.66	Min Vel: 0		

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.6	0.95	0.3	0.285	0.6	0.29
1	0.5	0.5	1.85	0.25	0.4625	0.6	0.46
1.5	0.5	0.8	2.24	0.4	0.896	0.6	0.90
2	0.5	0.9	2.4	0.45	1.08	0.6	1.08
2.5	0.5	1	2.31	0.5	1.155	0.6	1.16
3	0.5	1	2.09	0.5	1.045	0.6	1.05
3.5	0.5	0.9	2.13	0.45	0.9585	0.6	0.96
4	0.5	0.6	1.65	0.3	0.495	0.6	0.50
4.5	0.5	0.4	1.48	0.2	0.296	0.6	0.30
5	0.5	0.2	1.58	0.1	0.158	0.6	0.16
5.5	0.5	0.2	1.19	0.1	0.119	0.6	0.12
6	0.5	0.1	0	0.05	0	0.6	0.00
<b>total</b>	<b>4.5</b>	<b>7.2</b>	<b>19.87</b>	<b>3.55</b>			<b>4.213</b>
<b>average</b>	<b>0.5</b>	<b>0.6</b>	<b>1.655833</b>	<b>0.322727</b>			<b>0.741444</b>

6.95

note: measured flow with 006b flow. Subtracted 006b(2.737) from 007b total cfs(6.95)

El Dorado Chemical

date

5/4/2006

Start

1940

Stop

1950

Station:	006b EDCC			Level	1.3 at logger		
Waterbody Trib							
Crew:	JBB/JJF						
Width (ft):	4.5	Area:	1.8				
Flow (cfs):	2.74	Velocity:	1.22	Max Vel: 2.43 Min Vel: 0			

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.4	1.18	0.2	0.236	0.6	0.24
1	0.5	0.6	1.73	0.3	0.519	0.6	0.52
1.5	0.5	0.6	2.43	0.3	0.729	0.6	0.73
2	0.5	0.5	1.82	0.25	0.455	0.6	0.46
2.5	0.5	0.5	1.34	0.25	0.335	0.6	0.34
3	0.5	0.5	1.23	0.25	0.3075	0.6	0.31
3.5	0.5	0.3	0.68	0.15	0.102	0.6	0.10
4	0.5	0.2	0.53	0.1	0.053	0.6	0.05
4.5	0.5	0	0	0	0	0.6	0.00
<b>total</b>	<b>4.5</b>	<b>3.6</b>	<b>10.94</b>	<b>1.8</b>			<b>2.737</b>
<b>average</b>	<b>0.5</b>	<b>0.4</b>	<b>1.215556</b>	<b>0.2</b>			<b>0.304056</b>

El Dorado Chemical	date	5/4/2006	Start	1825
			Stop	1830
Station: 007b EDCC				
Waterbody Trib			Level	1.3 at logger
Crew: JBB/JJF				
Width (ft): 5.5	Area: 1.95	Max Vel: 2.14		
Flow (cfs): -0.09	Velocity: 1.49	Min Vel: 1.03		

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)	
0.5	0.5	0.4	1.08	0.2	0.216	0.6	0.22	
1	0.5	0.4	1.69	0.2	0.338	0.6	0.34	
1.5	0.5	0.4	2.02	0.2	0.404	0.6	0.40	
2	0.5	0.5	2.14	0.25	0.535	0.6	0.54	
2.5	0.5	0.6	2.08	0.3	0.624	0.6	0.62	
3	0.5	0.5	2.11	0.25	0.5275	0.6	0.53	
3.5	0.5	0.5	1.89	0.25	0.4725	0.6	0.47	
4	0.5	0.3	1.66	0.15	0.249	0.6	0.25	
4.5	0.5	0.2	1.03	0.1	0.103	0.6	0.10	
5	0.5	0.1	0.67	0.05	0.0335	0.6	0.03	
5.5	0.5	0	0	0	0	0.6	0.00	
total	4.5	3.9	16.37	1.95			-0.094	3.50
average	0.5	0.354545	1.488182	0.177273			0.385444	

note: measured flow with 006b flow. Subtracted 006b(3.597) from 007b total cfs(3.5)

El Dorado Chemical	date	5/4/2006	Start	1810
			Stop	1820
Station: 006b EDCC				
Waterbody Trib			Level	1.4 at logger
Crew: JBB/JJF				
Width (ft): 5	Area: 2.15	Max Vel: 2.4		
Flow (cfs): 3.60	Velocity: 1.26	Min Vel: 0		

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.5	0.92	0.25	0.23	0.6	0.23
1	0.5	0.5	1.48	0.25	0.37	0.6	0.37
1.5	0.5	0.6	2.12	0.3	0.636	0.6	0.64
2	0.5	0.7	2.4	0.35	0.84	0.6	0.84
2.5	0.5	0.7	1.8	0.35	0.63	0.6	0.63
3	0.5	0.6	1.87	0.3	0.561	0.6	0.56
3.5	0.5	0.4	1.35	0.2	0.27	0.6	0.27
4	0.5	0.2	0.49	0.1	0.049	0.6	0.05
4.5	0.5	0.1	0.21	0.05	0.0105	0.6	0.01
5	0.5	0	0	0	0	0.6	0.00
<b>total</b>	<b>4.5</b>	<b>4.3</b>	<b>12.64</b>	<b>2.15</b>			<b>3.597</b>
<b>average</b>	<b>0.5</b>	<b>0.43</b>	<b>1.264</b>	<b>0.215</b>			<b>0.399611</b>

El Dorado Chemical

date

6/17/2006

Start

1800

Stop

1805

Station:	007b EDCC			Level	0.82 at logger
Waterbody Trib					
Crew:	SKH/BJP				
Width (ft):	3.5	Area:	2	Max Vel:	0.65
Flow (cfs):	-0.25	Velocity:	0.49	Min Vel:	0

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.7	0.61	0.35	0.2135	0.6	0.21
1	0.5	0.8	0.58	0.4	0.232	0.6	0.23
1.5	0.5	0.8	0.63	0.4	0.252	0.6	0.25
2	0.5	0.6	0.6	0.3	0.18	0.6	0.18
2.5	0.5	0.6	0.65	0.3	0.195	0.6	0.20
3	0.5	0.4	0.36	0.2	0.072	0.6	0.07
3.5	0.5	0.1	0	0.05	0	0.6	0.00
<b>total</b>	<b>3.5</b>	<b>4</b>	<b>3.43</b>	<b>2</b>			<b>-0.251</b>
<b>average</b>	<b>0.5</b>	<b>0.571429</b>	<b>0.49</b>	<b>0.285714</b>			<b>0.1635</b>

1.14

note: measured flow with 006b flow. Subtracted 006b(1.395) from 007b total cfs(1.14)

El Dorado Chemical	date	6/17/2006	Start	1855
			Stop	1900
Station: 007b EDCC				
Waterbody Trib			Level	0.72 at logger
Crew: SKH/BJP				
Width (ft): 3.5	Area: 1.54	Max Vel: 0.36		
Flow (cfs): -0.16	Velocity: 0.25	Min Vel: 0		

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.6	0.28	0.3	0.084	0.6	0.08
1	0.5	0.7	0.34	0.35	0.119	0.6	0.12
1.5	0.5	0.7	0.35	0.35	0.1225	0.6	0.12
2	0.5	0.4	0.36	0.2	0.072	0.6	0.07
2.5	0.5	0.4	0.32	0.2	0.064	0.6	0.06
3	0.5	0.2	0.13	0.1	0.013	0.6	0.01
3.4	0.4	0.1	0	0.04	0	0.6	0.00
total	3.4	3.1	1.78	1.54		-0.156	0.47
average	0.485714	0.442857	0.254286	0.22		0.067786	

note: measured flow with 006b flow. Subtracted 006b(0.63) from 007b total cfs(0.47)

El Dorado Chemical                            date                            6/17/2006                            Start                            1750  
 Stop    1755  
 Station: 006b EDCC                            Level                            1.1 at logger  
 Waterbody Trib  
 Crew: SKH/BJP  
 Width (ft): 4                                  Area: 1.25                            Max Vel: 1.77  
 Flow (cfs): 1.40                               Velocity: 0.92                            Min Vel: 0

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.1	0	0.05	0	0.6	0.00
1	0.5	0.3	0.63	0.15	0.0945	0.6	0.09
1.5	0.5	0.4	1.27	0.2	0.254	0.6	0.25
2	0.5	0.4	1.14	0.2	0.228	0.6	0.23
2.5	0.5	0.5	1.08	0.25	0.27	0.6	0.27
3	0.5	0.4	1.77	0.2	0.354	0.6	0.35
3.5	0.5	0.3	1.2	0.15	0.18	0.6	0.18
4	0.5	0.1	0.29	0.05	0.0145	0.6	0.01
<b>total</b>	<b>4</b>	<b>2.5</b>	<b>7.38</b>	<b>1.25</b>			<b>1.395</b>
<b>average</b>	<b>0.5</b>	<b>0.3125</b>	<b>0.9225</b>	<b>0.15625</b>			<b>0.174375</b>

El Dorado Chemical                          date                          6/17/2006                          Start                          1850  
 Stop                          1855  
 Station: 006b EDCC                          Level                          1.00 at logger  
 Waterbody Trib  
 Crew: SKH/BJP  
 Width (ft): 3.5                  Area: 0.8                  Max Vel: 1.54  
 Flow (cfs): 0.63                  Velocity: 0.70                  Min Vel: 0

Distance from initial point (ft)	Width (ft)	Depth (ft)	Avg. velocity at point (ft/sec)	Area (sq. ft.)	Discharge (cfs)	Method Depth	Average Discharge (cfs)
0.5	0.5	0.1	0.6	0.05	0.03	0.6	0.03
1	0.5	0.3	1.11	0.15	0.1665	0.6	0.17
1.5	0.5	0.3	0.71	0.15	0.1065	0.6	0.11
2	0.5	0.3	0	0.15	0	0.6	0.00
2.5	0.5	0.3	1.54	0.15	0.231	0.6	0.23
3	0.5	0.2	0.96	0.1	0.096	0.6	0.10
3.5	0.5	0.1	0	0.05	0	0.6	0.00
<b>total</b>	<b>3.5</b>	<b>1.6</b>	<b>4.92</b>	<b>0.8</b>			<b>0.630</b>
<b>average</b>	<b>0.5</b>	<b>0.228571</b>	<b>0.702857</b>	<b>0.114286</b>			<b>0.09</b>

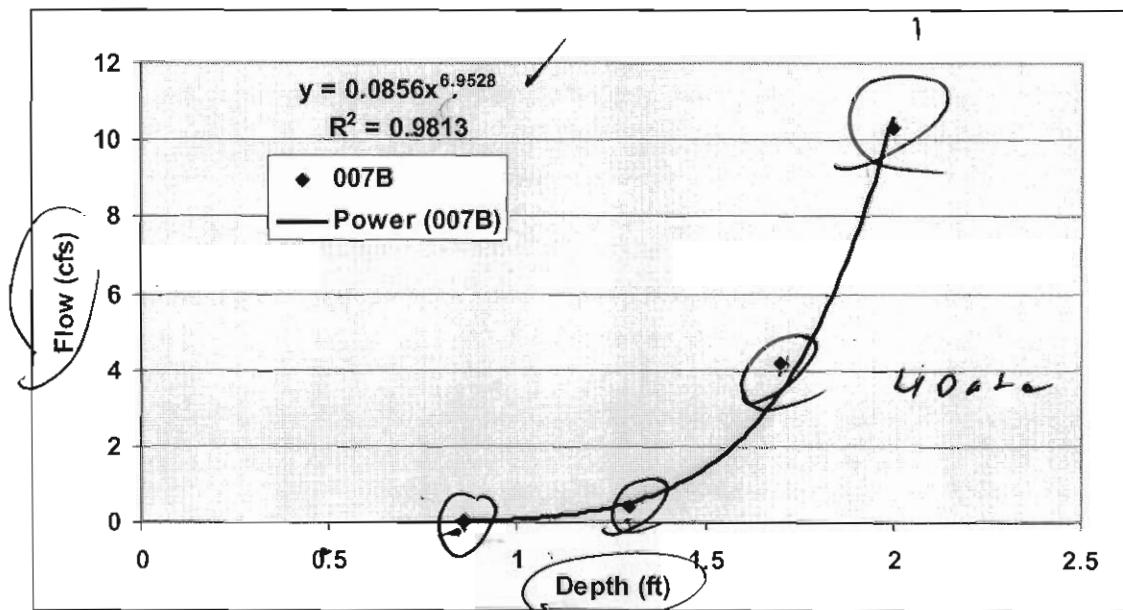
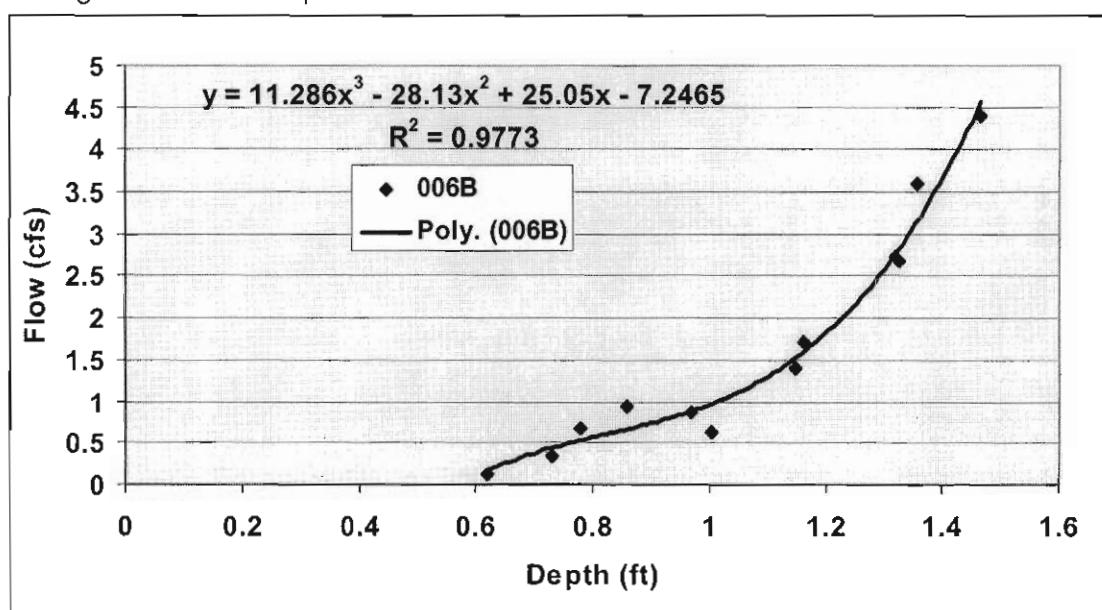
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**Appendix D**

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**Rating Curves**

Rating curves developed from field data.



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**Appendix E**

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**USDA Flume Tables**

H, ft	006 3ft H flume	
	FLOW MGD	FLOW CFS
0.01	0.0006	0.0009
0.02	0.0014	0.0022
0.03	0.0029	0.0045
0.04	0.0047	0.0073
0.05	0.0068	0.0105
0.06	0.0092	0.0142
0.07	0.012	0.0186
0.08	0.0151	0.0234
0.09	0.0186	0.0288
0.1	0.0224	0.0347
0.11	0.0263	0.0407
0.12	0.0304	0.0470
0.13	0.0348	0.0538
0.14	0.0394	0.0610
0.15	0.0443	0.0685
0.16	0.0495	0.0766
0.17	0.055	0.0851
0.18	0.0607	0.0939
0.19	0.0667	0.1032
0.2	0.073	0.1129
0.21	0.0795	0.1230
0.22	0.0866	0.1340
0.23	0.0937	0.1450
0.24	0.1008	0.1559
0.25	0.1086	0.1680
0.26	0.1163	0.1799
0.27	0.1247	0.1929
0.28	0.1338	0.2070
0.29	0.1442	0.2231
0.3	0.1512	0.2339
0.31	0.1609	0.2489
0.32	0.1706	0.2639
0.33	0.181	0.2800
0.34	0.1913	0.2960
0.35	0.2016	0.3119
0.36	0.2126	0.3289
0.37	0.2243	0.3470
0.38	0.2359	0.3650
0.39	0.2475	0.3829
0.4	0.2598	0.4019
0.41	0.2721	0.4210
0.42	0.285	0.4409
0.43	0.2986	0.4620
0.44	0.3122	0.4830

H, ft	007 4ft HL flume	
	FLOW MGD	FLOW CFS
0.01	0.001	0.0015
0.02	0.003	0.0046
0.03	0.0078	0.0121
0.04	0.0129	0.0200
0.05	0.0187	0.0289
0.06	0.0252	0.0390
0.07	0.0323	0.0500
0.08	0.0401	0.0620
0.09	0.0485	0.0750
0.1	0.0575	0.0890
0.11	0.0666	0.1030
0.12	0.0769	0.1190
0.13	0.0873	0.1351
0.14	0.0982	0.1519
0.15	0.1099	0.1700
0.16	0.1228	0.1900
0.17	0.1364	0.2110
0.18	0.1499	0.2319
0.19	0.1648	0.2550
0.2	0.1797	0.2780
0.21	0.1952	0.3020
0.22	0.2113	0.3269
0.23	0.2275	0.3520
0.24	0.2443	0.3780
0.25	0.2618	0.4050
0.26	0.2805	0.4340
0.27	0.3005	0.4649
0.28	0.3212	0.4969
0.29	0.3425	0.5299
0.3	0.3652	0.5650
0.31	0.3878	0.6000
0.32	0.4104	0.6349
0.33	0.433	0.6699
0.34	0.4556	0.7049
0.35	0.4783	0.7400
0.36	0.5041	0.7799
0.37	0.53	0.8200
0.38	0.5558	0.8599
0.39	0.5817	0.8999
0.4	0.6075	0.9399
0.41	0.6347	0.9819
0.42	0.6657	1.0299
0.43	0.698	1.0799
0.44	0.7239	1.1199





H, ft	006 3ft H flume	
	FLOW MGD	FLOW CFS
1.33	3.076	4.7589
1.34	3.128	4.8393
1.35	3.18	4.9198
1.36	3.232	5.0002
1.37	3.283	5.0791
1.38	3.335	5.1596
1.39	3.387	5.2400
1.4	3.445	5.3298
1.41	3.496	5.4087
1.42	3.555	5.4999
1.43	3.606	5.5788
1.44	3.665	5.6701
1.45	3.723	5.7599
1.46	3.774	5.8388
1.47	3.833	5.9300
1.48	3.891	6.0198
1.49	3.949	6.1095
1.5	4.007	6.1992
1.51	4.072	6.2998
1.52	4.13	6.3895
1.53	4.188	6.4793
1.54	4.253	6.5798
1.55	4.311	6.6695
1.56	4.375	6.7686
1.57	4.44	6.8691
1.58	4.498	6.9589
1.59	4.563	7.0594
1.6	4.628	7.1600
1.61	4.692	7.2590
1.62	4.757	7.3596
1.63	4.828	7.4694
1.64	4.892	7.5684
1.65	4.957	7.6690
1.66	5.028	7.7788
1.67	5.093	7.8794
1.68	5.164	7.9892
1.69	5.235	8.0991
1.7	5.3	8.1996
1.71	5.371	8.3095
1.72	5.442	8.4193

H, ft	007 4ft HL flume	
	FLOW MGD	FLOW CFS
1.33	6.528	10.0995
1.34	6.592	10.1985
1.35	6.722	10.3996
1.36	6.786	10.4986
1.37	6.915	10.6982
1.38	6.98	10.7988
1.39	7.109	10.9983
1.4	7.239	11.1995
1.41	7.368	11.3990
1.42	7.497	11.5986
1.43	7.562	11.6992
1.44	7.691	11.8987
1.45	7.82	12.0983
1.46	7.949	12.2979
1.47	8.014	12.3985
1.48	8.143	12.5980
1.49	8.273	12.7992
1.5	8.402	12.9987
1.51	8.531	13.1983
1.52	8.596	13.2989
1.53	8.725	13.4984
1.54	8.854	13.6980
1.55	8.984	13.8991
1.56	9.113	14.0987
1.57	9.242	14.2983
1.58	9.371	14.4979
1.59	9.501	14.6990
1.6	9.63	14.8986
1.61	9.759	15.0981
1.62	9.888	15.2977
1.63	10.02	15.5019
1.64	10.15	15.7031
1.65	10.28	15.9042
1.66	10.47	16.1981
1.67	10.6	16.3993
1.68	10.73	16.6004
1.69	10.86	16.8015
1.7	10.99	17.0026
1.71	11.12	17.2038
1.72	11.25	17.4049

## **Appendix F**

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### **Flow Event Summary Data**







PESTICIDES	Reported Value (Ce) (ug/l)	Ce'2.13 (ug/l)	EPA Acute (ug/l)	STATE Acute (ug/l)	IWC Acute (ug/l)	EPA Chronic (ug/l)	STATE Chronic (ug/l)	IWC Chronic (ug/l)	EPA Bioacc. (ug/l)	STATE Bioacc. (ug/l)	IWC Bioacc. (ug/l)	Violation of Acute Chr	Violation of Bio
104. Atrin	0.00	0.00	3.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00140	0.00	0.00	NO
105. Alpha-BHC	0.00	0.00	.....	2.00	0.00	.....	0.08	0.00	1.300E-01	0.0373	0.00	0.00	NO
106. Beta-BHC	0.00	0.00	.....	2.00	0.00	.....	0.08	0.00	0.4600	.....	0.00	0.00	NO
107. Gamma-BHC	0.00	0.00	2.00	2.00	0.00	0.08	0.08	0.00	0.6300	.....	0.00	0.00	NO
108. Delta-BHC	0.00	0.00	.....	2.00	0.00	.....	0.08	0.00	.....	.....	0.00	0.00	NO
109. Chlordane	0.00	0.00	2.40	2.40	0.00	0.0043	0.0043	0.00	5.900E-03	0.0050	0.00	0.00	NO
110. 4,4'-DDT	0.00	0.00	1.10	1.10	0.00	0.0010	0.0010	0.00	0.0059	.....	0.00	0.00	NO
111. 4,4'-DDE	0.00	0.00	.....	1.10	0.00	.....	0.0010	0.00	0.0059	.....	0.00	0.00	NO
112. 4,4'-DDD	0.00	0.00	.....	2.50	2.50	0.00	0.0019	0.0019	0.0084	.....	0.00	0.00	NO
113. Dieldrin	0.00	0.00	2.50	2.50	0.00	0.00560	0.00560	0.00	1.400E-03	0.0012	0.00	0.00	NO
114. Alpha-endosulfan	0.00	0.00	0.22	0.22	0.00	0.00560	0.00560	0.00	2.00	.....	0.00	0.00	NO
115. Beta-endosulfan	0.00	0.00	0.22	0.22	0.00	0.00560	0.00560	0.00	2.00	.....	0.00	0.00	NO
116. Endosulfan sulfate	0.00	0.00	.....	0.22	0.00	.....	0.00	0.00	2.00	.....	0.00	0.00	NO
117. Endrin	0.00	0.00	0.18	0.18	0.00	0.0023	0.0023	0.00	8.100E-01	.....	0.00	0.00	NO
118. Endrin aldehyde	0.00	0.00	0.18	0.18	0.00	0.0023	0.0023	0.00	8.100E-01	.....	0.00	0.00	NO
119. Heptachlor	0.00	0.00	0.52	0.52	0.00	0.0038	0.0038	0.00	0.0021	.....	0.00	0.00	NO
120. Heptachlor epoxide	0.00	0.00	0.52	0.52	0.00	0.0038	0.0038	0.00	0.0011	.....	0.00	0.00	NO
121. PCB-1242	0.00	0.00	.....	0.00	0.0140	0.0140	0.00	4.500E-04	4.000E-04	0.00	0.00	NO	NO
122. PCB-1254	0.00	0.00	.....	0.00	0.0140	0.0140	0.00	4.500E-04	4.000E-04	0.00	0.00	NO	NO
123. PCB-1221	0.00	0.00	.....	0.00	0.0140	0.0140	0.00	4.500E-04	4.000E-04	0.00	0.00	NO	NO
124. PCB-1232	0.00	0.00	.....	0.00	0.0140	0.0140	0.00	4.500E-04	4.000E-04	0.00	0.00	NO	NO
125. PCB-1248	0.00	0.00	.....	0.00	0.0140	0.0140	0.00	4.500E-04	4.000E-04	0.00	0.00	NO	NO
126. PCB-1260	0.00	0.00	0.00	0.0140	0.0140	0.00	4.500E-04	4.000E-04	0.00	0.00	0.00	NO	NO
127. PCB-1016	0.00	0.00	0.00	0.0140	0.0140	0.00	4.500E-04	4.000E-04	0.00	0.00	0.00	NO	NO
128. Toxaphene	0.00	0.00	0.73	0.73	0.00020	0.00020	0.00	4.500E-04	0.0063	0.00	0.00	NO	NO
130. Chlorpyrifos	0.00	0.083	0.083	0.041	0.041	0.00	0.00	0.00	.....	0.00	0.00	NO	NO

AWQ, Reg. No. 2	Reported Value (Ce) (µg/l)	Ce-2.13 (µg/l)	STATE Acute (µg/l)	IWC Acute (µg/l)	STATE Chronic (µg/l)	IWC Chronic (µg/l)	STATE Bioacc. (µg/l)	IWC Bioacc. (µg/l)	Violation of Bio
									Acute Chr
Alpha-BHC	0.00	0.00	2.00	0.00	0.08	0.00	0.0373	0.00	NO NO NO
Beta-BHC	0.00	0.00	2.00	0.00	0.08	0.00	0.010	0.00	NO NO NO
Gamma-BHC	0.00	0.00	2.00	0.00	0.08	0.00	0.010	0.00	NO NO NO
Delta-BHC	0.00	0.00	2.00	0.00	0.08	0.00	0.010	0.00	NO NO NO
Pentachlorophenol	0.00	0.00	11.78	0.00	7.44	0.00	0.00	0.00	NO NO NO
Aldrin	0.00	0.00	3.00	0.00	0.00	0.00	0.0019	0.00	NO NO NO
Chlordane	0.00	0.00	2.40	0.00	0.043	0.00	0.005	0.00	NO NO NO
4,4'-DDT	0.00	0.00	1.10	0.00	0.010	0.00	0.00	0.00	NO NO NO
4,4'-DDE	0.00	0.00	1.10	0.00	0.010	0.00	0.00	0.00	NO NO NO
4,4'-DDD	0.00	0.00	1.10	0.00	0.010	0.00	0.00	0.00	NO NO NO
Dieldrin	0.00	0.00	2.50	0.00	0.00	0.00	0.0012	0.00	NO NO NO
Alpha-endosulfan	0.00	0.00	0.22	0.00	0.0560	0.00	0.00	0.00	NO NO NO
Beta-endosulfan	0.00	0.00	0.22	0.00	0.0560	0.00	0.00	0.00	NO NO NO
Endosulfan sulfate	0.00	0.00	0.22	0.00	0.0560	0.00	0.00	0.00	NO NO NO
Endrin	0.00	0.00	0.18	0.00	0.00	0.00	0.0023	0.00	NO NO NO
Endrin aldehyde	0.00	0.00	0.18	0.00	0.00	0.00	0.00	0.00	NO NO NO
Heptachlor	0.00	0.00	0.52	0.00	0.0038	0.00	0.00	0.00	NO NO NO
Heptachlor epoxide	0.00	0.00	0.52	0.00	0.0038	0.00	0.00	0.00	NO NO NO
Toxaphene	0.00	0.00	0.73	0.00	0.0002	0.00	0.0063	0.00	NO NO NO
Chlorpyrifos	0.00	0.00	0.083	0.00	0.0410	0.00	0.00	0.00	NO NO NO
Cadmum Total*	0.00	0.00	4.37	0.00	1.82	0.00	0.00	0.00	NO NO NO
Chromium (hex)	0.00	0.00	15.71	0.00	10.58	0.00	0.00	0.00	NO NO NO
Copper Total*	0.00	0.00	14.79	0.00	10.93	0.00	0.00	0.00	NO NO NO
Lead Total*	68.90	146.76	87.29	24.67	3.40	13.28	0.00	0.00	Yes
Mercury Total*	0.00	0.00	6.70	0.00	0.0120	0.00	0.00	0.00	NO NO NO
Nickel Total*	0.00	0.00	1061.45	0.00	117.88	0.00	0.00	0.00	NO NO NO
Selenium Total	0.00	20.00	5.00	0.00	0.00	0.00	0.00	0.00	NO NO NO
Silver Total*	0.00	1.5097	0.00	0.00	0.00	0.00	0.00	0.00	NO NO NO
Zinc Total*	471.00	1003.23	130.87	188.61	119.50	90.79	0.00	0.00	Yes NO
Chromium (Tri)*	0.00	0.00	1006.35	0.00	326.45	0.00	0.00	0.00	NO NO NO
Cyanide Total	0.00	0.00	22.36	5.20	0.00	0.00	0.00	0.00	NO NO NO
Beryllium Total	0.00	0.00	0.00	0.00	0.076	0.00	0.00	0.00	NO NO NO
PCB-1242	0.00	0.00	0.0140	0.00	4.00E-04	0.00	0.00	0.00	NO NO NO
PCB-1254	0.00	0.00	0.0140	0.00	4.00E-04	0.00	0.00	0.00	NO NO NO
PCB-1221	0.00	0.00	0.0140	0.00	4.00E-04	0.00	0.00	0.00	NO NO NO
PCB-1232	0.00	0.00	0.0140	0.00	4.00E-04	0.00	0.00	0.00	NO NO NO
PCB-1248	0.00	0.00	0.0140	0.00	4.00E-04	0.00	0.00	0.00	NO NO NO
PCB-1260	0.00	0.00	0.0140	0.00	4.00E-04	0.00	0.00	0.00	NO NO NO
PCB-1016	0.00	0.00	0.0140	0.00	4.00E-04	0.00	0.00	0.00	NO NO NO
2,3,7,8-TCDD	0.00	0.00	1E-06	0.00	0.00	0.00	0.00	0.00	NO NO NO

\* See Linear Partition Coefficient (Page 6)

#### AQUATIC LIFE CRITERIA (DISSOLVED ACUTE VALUES)

**Linear Partition Coefficients**

Metals	K <sub>po</sub>	Streams	a	Pollutant	Dissolved(ug/l)	Formula
Arsenic	.....		-0.73	Cadmium	1.04 WER X Conversion Factor" X e[1.128ln(hardness)]-3.828	
Cadmium	.....		-1.13	Chromium(III)	210.28 WER X 0.316 X e[0.819ln(hardness)]+3.688	
Chromium(3)	.....		-0.93	Chromium(V)	15.71 WER X 0.982 X 16	
Copper	.....		-0.74	Copper	5.64 WER X 0.96 X e[0.942ln(hardness)]-1.464	
Copper	.....		-0.80	Lead	17.68 WER X Conversion Factor" X e[1.273ln(hardness)]-1.460	
Lead	.....		-1.14	Mercury	2.04 WER X 0.85 X 2.4	
Mercury	.....		-0.57	Nickel	525.50 WER X 0.998 X e[0.8460ln(hardness)]+3.3612	
Nickel	.....		-0.70	Silver	0.4602 WER X 0.85 X e[1.77ln(hardness)]-6.52	
Zinc	.....		-1.03	Zinc	42.43 WER X 0.978 X e[0.8473ln(hardness)]+0.8604	
Silver	.....				" 1.136672 - [(ln hardness)(0.041838)]	
					" 1.46203 - [(ln hardness)(0.145712)]	

$$K_p = K_{po} \times TSS^{\alpha}$$

$K_p$  = Linear Partition Coefficient

TSS = Total Suspended Solids (mg/l)

$K_{po}$  = found from above table

$\alpha$  = found from above table

#### AQUATIC LIFE CRITERIA (DISSOLVED CHRONIC VALUES)

**C / C<sub>t</sub> = Fraction of Metal Dissolved**

Metals	Streams	C / C <sub>t</sub>	Pollutant	Dissolved(ug/l)	Formula
Arsenic	.....		Cadmium	0.43 WER X Conversion Factor" X e[0.785ln(hardness)]-3.490	
Cadmium	.....		Chromium(III)	68.21 WER X 0.86 X e[0.819ln(hardness)]+1.561	
Chromium (3)	.....		Chromium(V)	10.58 WER X 10	
Copper	.....		Copper	4.17 WER X 0.96 X e[0.8545ln(hardness)]-1.465	
Lead	.....		Lead	0.69 WER X Conversion Factor" X e[1.273ln(hardness)]-4.705	
Nickel	.....		Nickel	58.42 WER X 0.997 X e[0.8460ln(hardness)]+1.1645	
Zinc	.....		Zinc	38.74 WER X 0.986 X e[0.8473ln(hardness)]+0.7614	
				" 1.101672 - [(ln hardness)(0.041838)]	
				" 1.46203 - [(ln hardness)(0.145712)]	

Total Metal = Dissolved Metal / (C / C<sub>t</sub>)

EL DORADO CHEMICAL - AR00000752  
 DMR DATA FROM 03/01/05 THROUGH PRESENT  
 (LORETTA REIBER/PCS=>LORETTA)

\*\*\*\*\*  
 \*\*\*\*\* GENERAL FACILITY INFORMATION \*\*\*\*\*  
 \*\*\*\*\*  
 PERMIT NUMBER: AR00000752 PERMIT NUMBER: AR00000752  
 PAGE: 1

FACILITY NAME: EL DORADO CHEMICAL CO, INC.  
 (SEGMENT 2):  
 (SEGMENT 3):  
 (SEGMENT 4):  
 CITY : 28080 EL DORADO  
 COUNTY: 139 UNION  
 STATE : AR REGION: 06 SUB-REGION:  
 USGS HYD BAS CD: 08040202 STREAM SEGMENT: 0070 AVERAGE DESIGN FLOW : 2.431 CONTROL AUTHORITY ID :  
 USGS DESC: LOWER OUACHITA-BAYOU DE LOUTRE FEDERAL GRANT INDICATOR : RECEIVING POTW ID : RDF1: RDF4: 085 RDF7: STATE  
 RECEIVING STREAM CLASS CD: MILEAGE INDICATOR : FINAL LIMIT INDICATOR : RDF2: T RDF5: 2D RDF8: GREG  
 RECEIVING WATERS: TRIB/FLAT CK HAYNES CK OUACHITA RV WATER QUALITY LIMIT IND : PRETREAT PGM REQUIRED : RDF3: RDF6: RDF9:  
 LATITUDE : +3315250 LONGITUDE: -09241200 ATTORNEY: ENGINEER : LR RDF0: 7000040  
 LAT/LON CODE OF ACCURACY:

LAT/LON METHOD: U UNKNOWN TYPE OF OWNERSHIP: PRV PRIVATE  
 LAT/LON SCALE: U UNKNOWN SIC CODE/DESCRIP: 2873 NITROGEN FERTILIZERS  
 SLUDGE INDICATOR: F  
 SLUDGE CLASS FAC IND: PREVIOUS RATING: MINOR INDUSTRIAL CLASS : R ON EIG  
 SLUDGE USER DEFINED ELEMENT 1: ACTIVITY STATUS: ACTIVE CODE OF FED. REG.: 41BB AMMONIA  
 ARCHIVAL DESCRIPTOR: LAST ARCHIVAL DATE: 12/31/00 PERMIT DATE ISSUED: 05/31/02 PERMIT DATE EXPIRED: 06/30/07  
 NEW SOURCE CODE: ORIGINAL PERMIT ISSUE DATE: 10/22/74 REISSUED NUMBER:  
 \* MAILING INFORMATION \*

FACILITY LOCATION:  
 PRIMARY DMR MAILING ADDRESS: ALTERNATE DMR MAILING ADDRESS:

EL DORADO CHEMICAL CO, INC.  
 4500 NORTHWEST AV ANNUAL DRY SLUDGE PROD: 0000000 DMT/YR  
 (SEC-7 TMP-17S RNG-15W)  
 EL DORADO SLUDGE RELATED PERMIT #: 2:  
 ARKANSAS OPERATOR'S ADDRESS: 71730

SLUDGE COMMERCIAL HANDLER ADDRESS:

OWNER'S PHONE: OPERATORS'S PHONE: COGNIZANT OFFICIAL: WES MORGAN MGR ENVIRON COMPL  
 OFFICIAL'S PHONE: (870) 863-1484

EL DORADO CHEMICAL - AR0000752  
 DMR DATA FROM 03/01/05 THROUGH PRESENT  
 (LORETTA REIBER/PCS=>LORETTA)

\*\*\*\*\*  
 FACILITY: EL DORADO CHEMICAL CO, INC  
 PERMIT TYPE: STANDARD

TYPE OF APPLICATION: SC SHORT C  
 PERMIT ISSUED BY : S STATE

\* PERMIT TRACKING DATA \*

PERMIT NUMBER: AR0000752

PAGE: 2

PERMIT CODE / DESCRIPTION	TRACKING EVENT	ACTUAL DATE	SCHEDULED DATE	PERMIT TRACKING EVENT COMMENTS	NEW SOURCE CODE:	NUMBER OF REISSUES :	RDE1	RDE2
P10-99 APPLICATION RECEIVED		12/21/06						
P20-99 APPLICATION COMPLETE		01/02/07						
P30-99 DRAFT PERMIT/PUBLIC NOTICE		03/22/06						
P40-99 PERMIT ISSUED		05/31/02						
P50-99 PERMIT EXPIRED		06/30/07						
P60-99 PERMIT EFFECTIVE		07/01/02						
P70-99 STAYS		06/27/02		ENTIRE PERMIT APPEALED		02-004		
033-06 APPLICATION TO STATE		08/12/80						
034-06 DRAFT PERMIT RECD FROM STATE		03/05/90						
200-99 (REIS) PERMIT REISSUED		05/31/02						
300-99 PERMIT MODIFIED		04/30/04						
310-99 MODIFICATION REQUEST		01/12/05						
350-99 MODIFICATION PUBLIC NOTICE		01/15/04						
360-99 MODIFICATION EFFECTIVE		06/01/04						
600-99 APPLICATION SOLICITATION		02/21/85						
907-99 STATE CERTIFICATION REQUEST		12/04/82						

EL DORADO CHEMICAL - AR0000752  
 DMR DATA FROM 03/01/05 THROUGH PRESENT  
 (LORETTA REIBER/PCS=>LORETTA)

QL	006A 03/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	1.7	1.7	E00
006A 04/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	2.6		E00	
006A 05/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P			E00	
006A 05/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1			E00	
006A 06/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P			E00	
006A 06/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1			E00	
006A 07/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P	1.8	1.8	E00	
006A 08/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	0.851	0.851	E00	
006A 09/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	0.054	0.054	E00	
006A 10/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P			E00	
006A 11/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	0.70	0.85	E00	
006A 12/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	1.25	1.25	E00	
006A 01/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	1.0	1.0	E00	
006A 02/28/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1			E00	
006A 03/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P			E00	
006A 04/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1			E00	
006A 05/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P			E00	
006A 05/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1			E00	
006A 06/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P			E00	
006A 06/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	0.25	0.25	E00	
006A 07/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	0.020	0.025	E00	
006A 08/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1	2.8	3.2	E00	
006A 09/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1			E00	
006A 10/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 P			E00	
006A 11/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT	50050 1			E00	

SUB-TOTAL QUICK LOOK PRINT LINES:

31

10/05 - Study shows no rainfall or discharge  
 Other studies showed SW study shows discharge

EL DORADO CHEMICAL - AR0000752  
 DMR DATA FROM 03/01/05 THROUGH PRESENT  
 (LORETTA REIBER/PCS=>LORETTA)

QL \*\*\*\* QL  
 007A 03/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 2.2 2.2 E00  
 007A 04/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 2.9 2.9 E00  
 007A 05/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 05/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 05/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 06/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 06/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 07/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 08/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 09/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 10/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 11/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 11/30/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 12/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 12/31/05 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 01/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 02/28/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 03/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 04/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 05/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 05/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 06/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 06/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 07/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 08/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 09/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00  
 007A 09/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 10/31/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 1 E00  
 007A 11/30/06 FLOW, IN CONDUIT OR THRU TREATMENT PLANT 50050 P E00

SLL DOUG  
 SUB-TOTAL QUICK LOOK PRINT LINES:

31





219 Brown Lane

Bryant, AR 72022

(501) 847-7077

(501) 847-7943 fax



September 21, 2006

Mr. Martin Maner, P.E., Chief  
Water Division  
Arkansas Department of Environmental Quality  
P.O. Box 8913  
Little Rock, AR 72219-8913

Re: Storm Water Flow Study Report - El Dorado Chemical Company  
GBM<sup>c</sup> No. 2042-99-010

Mo \_\_\_\_\_  
Have Staff review and  
make changes you feel  
are appropriate.

Noting - 9-26-06  
GRETA: (LDS)

Dear Mr. Maner:

As required by Item 12 in Part III of NPDES Permit No. AR0000752, please find enclosed the Storm Water Flow Study Report for El Dorado Chemical Company.

If you have any questions, do not hesitate to contact me or Wes Morgan, El Dorado Chemical Company.

Sincerely,  
GBM<sup>c</sup> & ASSOCIATES

*Chuck Campbell*  
Chuck Campbell, PE, REM  
Senior Engineer

Attachments

CC: Mo Shafii, ADEQ  
John Carver, LSB Industries  
Wes Morgan, EDCC



**Clem, Sarah**

---

**From:** Clem, Sarah  
**Sent:** Friday, December 08, 2006 11:52 AM  
**To:** Reiber, Loretta; Shafii, Mo; Roberts, Christopher; Singleton, Bob  
**Subject:** EDCC Storm flow study Outfalls 006/007 comments

007

When reviewing the reported Pb concentrations they are very high. In March 2006, 68.9 ug/L was reported from outfall 007. This was measured during a period EDCC recommended the limits be removed. EDCC is also reporting concentrations for Zn which exceed limitations during the period they recommend limits be removed.

006

Concentrations reported for both Pb and Zn are not as high as Outfall 007 however most are 3 times the limitation. The EDCC recommended limitations for Pb and Zn from November to June are similar to concentrations for a discharge into a large river.

I recommend the source of Pb, and Zn be removed or some treatment alternative be evaluated prior to a significant change in limits. This discharge would be toxic if EDCC recommendations are followed.

„ Sarah Clem  
Program Support Manager  
ADEQ  
8001 National Dr.  
P.O. Box 8913  
Little Rock, AR 72219-8913  
T: 501.682.0663  
F: 501.682.0910

**Reiber, Loretta**

---

**From:** Shafii, Mo  
**Sent:** Thursday, August 10, 2006 11:02 AM  
**To:** Reiber, Loretta  
**Subject:** FW: EDCC EQ Basin Temperature Study (follow up question)

Thanks

*Mo Shafii  
Permits Section Chief  
NPDES, Water Division  
Arkansas Department of Environmental Quality  
Telephone: 501-682-0616  
Fax: 501-682-0910  
E-Mail: shafii@adeg.state.ar.us*

-----Original Message-----

**From:** Shafii, Mo  
**Sent:** Monday, February 27, 2006 2:04 PM  
**To:** Singleton, Bob  
**Subject:** RE: EDCC EQ Basin Temperature Study (follow up question)

What is the next step. Do you need to go to PN or what?

Thanks

Mo

-----Original Message-----

**From:** Singleton, Bob  
**Sent:** Monday, February 27, 2006 12:43 PM  
**To:** Shafii, Mo  
**Subject:** RE: EDCC EQ Basin Temperature Study (follow up question)

That's ok.

-----Original Message-----

**From:** Shafii, Mo  
**Sent:** Monday, February 27, 2006 11:35  
**To:** Singleton, Bob  
**Subject:** FW: EDCC EQ Basin Temperature Study (follow up question)

Bob;

What do you think about the response to your request.

Thanks

Mo

-----Original Message-----

**From:** Shon Simpson [mailto:[ssimpson@gbmcassoc.com](mailto:ssimpson@gbmcassoc.com)]

**Sent:** Monday, February 27, 2006 11:07 AM  
**To:** Shafii, Mo  
**Cc:** Vince Blubaugh  
**Subject:** EDCC EQ Basin Temperature Study (follow up question)

Mo, I apologize for not getting back to you quicker regarding the selection of Captain Black Lake for comparison purposes with the EDCC EQ Basin. I understand from previous conversation that my email of February 7 (below) satisfied the questions that you posed in your letter of February 2, 2006 to Vince. The remaining question was why a Red River oxbow used instead of one along the Ouachita River. The reasons for use of Captain Black Lake were: (1) It was of generally similar morphology as the EDDC EQ Basin. The EQ Basin is approximately 2500 ft. long and 1000 ft. wide at its widest point, generally covers 50 acres and is 4 ft. deep in its shallow end and greater than 10 ft. deep toward the dam. Captain Black is slightly larger at 59 acres, is approximately 3000 ft. long and 1200 ft. wide at its widest point and was also 4 ft. deep in its shallow end and greater than 10 ft. deep. (2) The two waterbodies are near the same latitude, and probably most importantly, (3) Captain Black Lake is on private property with a locked gate. Without control of access to the lake we could not assure that the study equipment that collected the data for the project would have survived the study, or even a small portion of it. Because the temperature probes had to be suspended from the surface, (to maintain consistent measurement depth) the floats used to suspend the probes were highly visible and it would have not been possible to maintain the devices in an uncontrolled situation.

Although we did not conduct an exhaustive search, we were not able to match the attributes of Captain Black Lake as a control condition for the EDCC EQ Basin. Therefore, it was selected as the control lake and was included by name in the Workplan approved to conduct the study.

Please let me know if this satisfies the remaining question on the study. Thanks Shon

>>> "Shafii, Mo" <SHAFII@adeq.state.ar.us> 2/8/2006 4:11 PM >>>

Shon:

FYI

-----Original Message-----

**From:** Singleton, Bob  
**Sent:** Wednesday, February 08, 2006 15:18  
**To:** Harmon, Jennifer  
**Subject:** RE: EDCC EQ Basin Temperature Study

Although we don't sample that lake as a part of our lakes assessment, it would have the same designated uses as the other lakes in the state, with the same water quality protection mechanism. Why did they do a study on a Red River oxbow, and not one along the Ouachita River, where EDCC is located?

-----Original Message-----

**From:** Shon Simpson [mailto:[ssimpson@gbmcassoc.com](mailto:ssimpson@gbmcassoc.com)]  
**Sent:** Tuesday, February 07, 2006 4:41 PM



219 Brown Lane

Bryant, AR 72022

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(501) 847-7943 fax

February 1, 2007

FEB - 2 2007

sw

Mr. Mo Shafii  
 Permits Section Chief  
 NPDES Section, Water Division  
 Arkansas Department of Environmental Quality  
 8001 National Drive  
 PO Box 8913  
 Little Rock, AR 72219-8913

NPDES PERMIT FILE

NPDES # AR0000752AFIN # 70-00040

Permit PN

 Correspondence

Technical Backup

2-2-07 sw Date Scanned

RE: El Dorado Chemical Company, NPDES AR0000752, AFIN 70-00040  
 GBM<sup>c</sup> No. 2042-99-010

Dear Mr. Shafii:

El Dorado Chemical Company (EDCC) has received your letter dated January 5, 2007 regarding the Storm Water Flow Study Report prepared by GBM<sup>c</sup> & Associates and has asked us to prepare a response. Please consider the following regarding your concerns listed in the January 5 letter.

1. From Figure 1 on Page 2 of the Report, it appears that the background flow meters were placed downstream of Outfalls 006 and 007. If this is correct, please explain why this is appropriate. Also, please explain why monitors were not also placed at the property boundary upstream of the facility to determine the flow rate of the stream entering the property.

*Response: Monitoring stations were established according to the Storm Water Flow Study Plan dated July 15, 2004 and the Addendum dated September 17, 2004 which was approved by ADEQ. The September addendum (attached) explains the placement of monitoring stations for Outfalls 006 and 007.*

2. Section 5.1 of the Report:

- a. It is not clear whether the background flow to effluent flow ratios were assumed to be normally distributed in the confidence interval calculations. Please provide the assumptions made and a detailed copy of the calculations for the lower 95% confidence interval proposed (i.e., reference citations and equations used).
- b. Please explain why days without rainfall were not included in the calculations.
- c. Please explain why the lower 95% confidence interval will be protective of human health and the environment versus a more restrictive interval (e.g., lower 99.99% confidence interval). Is there any regulatory basis or precedent to the proposed confidence interval?

*Response a: The distribution of each data set were not normally distributed. However, the confidence intervals for each mean were calculated using a two-sided 100(1-a)% confidence interval that typically is associated with normal distributions. The equation for the lower confidence interval is presented below.*

$$X - t_{1-\alpha/2, n-1 \text{ df}} * SE$$

*This equation was chosen for use in this case as it generally provides a more conservative value than a distribution free statistical method and is the procedure commonly used in statistical software packages. In the case of these data sets this generality holds true. Lower 95% CI's calculated by a distribution free method results in more liberal values of 54.5 and 15.3, for the 006 Seasonal and 007 Seasonal values, respectively.*

*Response b: The objective of the study was to establish the ratio of facility storm effluent to the receiving stream flow. The study lasted 472 days, during which time data was logged at four locations in five-minute intervals, for an approximate total of 540,000 data points. To minimize the processing of useless information, data points that did not include coincident measurable flows from both outfalls 006/007 and the receiving stream were excluded from the statistical analysis.*

*Response c: The lower 95% CI provides a measure of conservatism beyond the mean, ensuring that atypical years with smaller rain events are still protective of in-stream water quality. The 95 percentile probability basis ( $\alpha=0.05$ ) is consistent with ADEQ permitting practice for calculation of average monthly limits for toxics.*

**3. It is important to note that the final background flow to effluent flow ratio for each outfall will be included in the permit upon renewal. Please explain how compliance with these proposed limits will be met and monitored.**

*Response: The study was based on several events across a fifteen-month period and demonstrates a conservative relationship between the facility storm effluent and receiving stream flows. The recommendations used study findings and considered the range of flow ratios exhibited to request permit conditions that will be protective of water quality using the 95 percentile probability. To avoid burdensome and unnecessary monitoring and reporting, EDCC suggests that the seasonal (November – June) flow relationships be verified once prior to renewal of the current NPDES permit, and once during each subsequent renewed permit cycle. Verification of the ratios will be provided to ADEQ in a summary report describing the event conditions and flow ratios observed during the field verification. EDCC is opposed to institution of flow ratios as a permit limit on an uncontrolled, natural drainage system. Inclusion of ratios as a permit limit infers that EDCC has the ability to manipulate storm effluent through outfalls 006 and 007, which it does not. Again, the purpose of the Storm Water Flow Study was to determine what ratios were observed and provide that data to ADEQ for use in determining appropriate permit limits for storm water discharges.*

Mr. Mo Shafii, ADEQ  
February 1, 2007  
Page 3

We appreciate the opportunity to provide supporting information to you on this matter on behalf of EDCC. We propose to meet with you and your staff as soon as possible to discuss this response and any other issues you may have concerning the Storm Water Flow Study Report and recommendations. I will contact you to schedule a convenient meeting time, but if you have immediate questions please contact me at 501-847-7077.

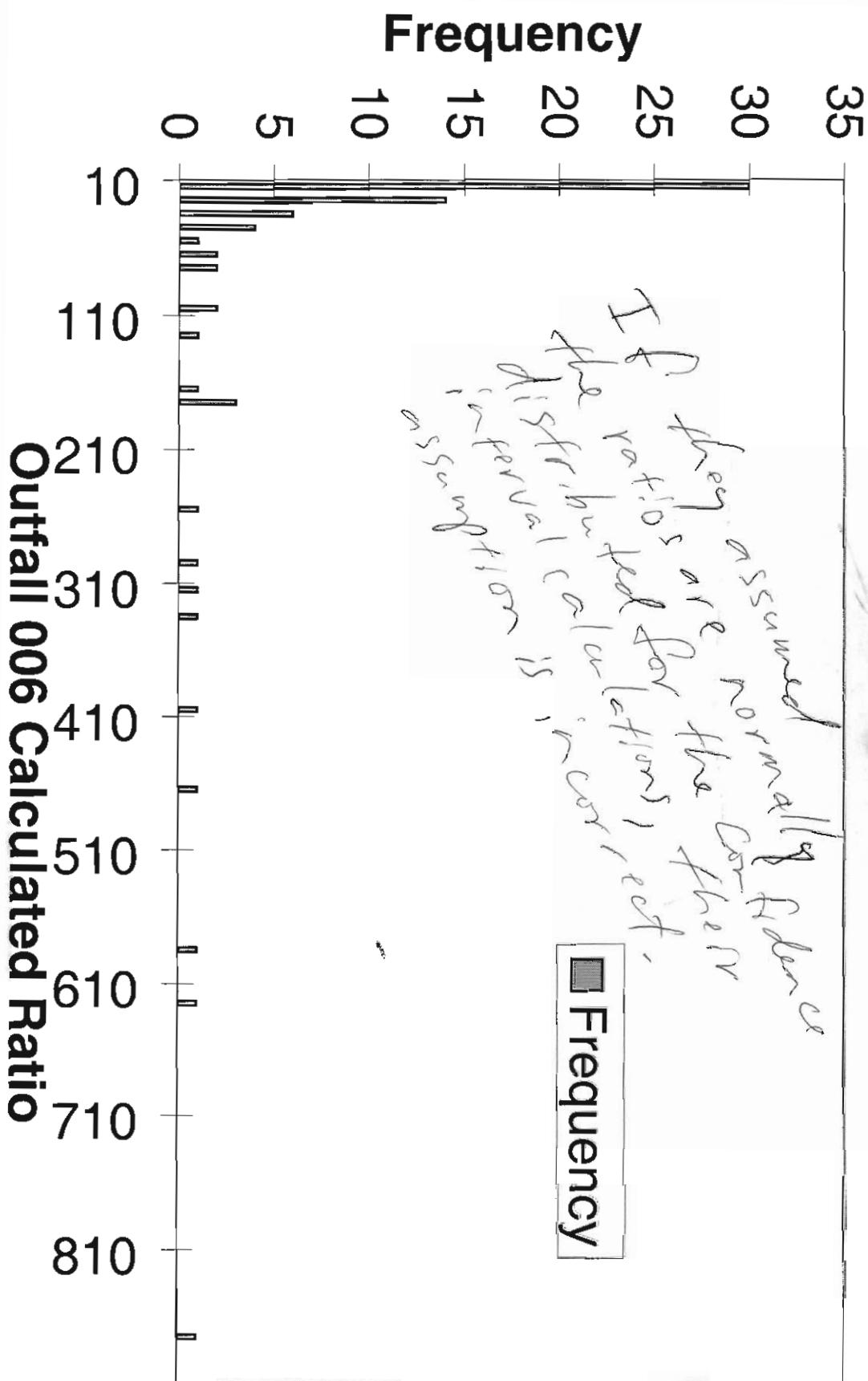
Sincerely,  
GBM<sup>c</sup> & Associates



Chuck Campbell, PE, REM  
Principal/Senior Engineer

cc:  
attach      Martin Maner – ADEQ  
                John Carver – LSB  
                Greg Withrow - EDCC  
                Brent Parker – EDCC

# Histogram



## **SECTION B. SCHEDULE OF COMPLIANCE**

The permittee shall achieve compliance with the effluent limitations specified for discharges in accordance with the following schedule:

### **Outfalls 001, 002, 003, 004, 005, 006, and 007:**

1. Compliance with interim limitations is required on the effective date of the permit.
2. The permittee shall achieve compliance with final limitations in accordance with the following:

Activity	Compliance Date from
1. Submit Progress Report	Effective date of the modified permit
2. Submit Progress Report	One Year
3. Achieve final limitations	Two Years

3. Consent Administrative Order No. 02-059 continues to remain in effect and provides the permittee three(3) years from the effective date of this permit to comply with technology-based limits contained herein.

### **Outfalls 010 or 011 (Combined flows of Outfalls 001, 002, and 004):**

1. Compliance with final limitations is required on the effective date of the permit. Permittee must notify ADEQ in writing ten days after operation of outfall 010 or 011 in order to terminate outfalls 001, 002 and 004.

### **Outfalls 002, 004, 005, 006, and 007 - Item #12 in Part III**

1. Within 90 days of permit issuance, the permittee shall submit a protocol for the evaluation of the background flow of the receiving streams for these outfalls and the dilution of the effluent in the receiving stream as a result of a storm event.
2. The evaluation shall be completed within 18 months of permit issuance.
3. Until such time as the permit is reopened and modified, the effluent limits and toxicity testing requirements in this permit remain in effect.

### **Outfall 001 - Item #1 in Part III**

1. Within 90 days of permit issuance, the permittee shall submit a protocol for the evaluation of the temperature regime of the fifty (50) acre equalization basin for the purpose of determining if the elevation of the temperatures in the equalization basin are related to ambient sources of heat resulting from summertime conditions.
2. The evaluation shall be completed within 18 months of permit issuance.

13. The sampling frequency for dissolved minerals at all outfalls shall be reduced automatically to once per quarter after 24 consecutive months with no violations. If a violation occurs after the frequency has been reduced, the monitoring frequency will then automatically increase back to once per month. However, if a violation of the dissolved minerals effluent limitations occurs at Outfall 001 while the permittee is monitoring once per month, the frequency shall then be increased to three times per week.
14. The permittee shall perform an evaluation of the temperature regime of the fifty (50) acre equalization basin for the purpose of determining if the elevation of temperatures in the equalization basin are related to ambient sources of heat resulting from summertime conditions. This permit may be modified to remove the temperature limitation for Outfall 001 if the evaluation documents that the elevation of water temperatures in the fifty (50) acre equalization basin are related to ambient sources of heat under summertime conditions.

15. **WHOLE EFFLUENT TOXICITY TESTING (48-HOUR ACUTE NOEC FRESHWATER)**

1. **SCOPE AND METHODOLOGY**

- a. The permittee shall test the effluent for toxicity in accordance with the provisions in this section.

APPLICABLE TO FINAL OUTFALLS: **002, 004, 005, 006, and 007**

CRITICAL DILUTION (%): **100%** (all outfalls in this condition)

EFFLUENT DILUTION SERIES (%): **32%, 42%, 56%, 75%, 100%**

COMPOSITE SAMPLE TYPE: Defined at PART I

TEST SPECIES/METHODS: 40 CFR Part 136

Daphnia pulex acute static renewal 48-hour definitive toxicity test using EPA/600/4-90/027F, or the latest update thereof. A minimum of five (5) replicates with eight (8) organisms per replicate must be used in the control and in each effluent dilution of this test.

Pimephales promelas (fathead minnow) acute static renewal 48-hour definitive toxicity test using EPA/600/4-90/027F, or the latest update thereof. A minimum of five (5) replicates with eight (8) organisms per replicate must be used in the control and in each effluent dilution of this test.

- b. The NOEC (No Observed Effect Concentration) is defined as the greatest effluent dilution above which lethality that is statistically different from the control (0%effluent) at the 95% confidence level does not occur.